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FLORIDA INTERNATIONAL UNIVERSITY

Miami, Florida

THE DISCRIMINATION AND ASSOCIATION OF FLOAT GLASS AND THE QUANTITATIVE ANALYSIS OF LIQUIDS FROM AEROSOLS AND MICRODROPS USING LASER INDUCED BREAKDOWN SPECTROSCOPY

A dissertation submitted in partial fulfillment of

the requirements for the degree of

DOCTOR OF PHILOSOPHY

in

CHEMISTRY

by

Erica M. Cahoon

To: Dean Kenneth G. Furton College of Arts and Sciences

This dissertation, written by Erica M. Cahoon, and entitled The Discrimination and Association of Float Glass and The Quantitative Analysis of Liquids from Aerosols and Microdrops using Laser Induced Breakdown Spectroscopy, having been approved in respect to style and intellectual content, is referred to you for judgment.

We have read this dissertation and recommend that it be approved.

Yong Cai

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Date of Defense: April 10, 2012

The dissertation of Erica M. Cahoon is approved.

Dean Kenneth G. Furton College of Arts and Sciences

Dean Lakshmi N. Reddi University Graduate School

Florida International University, 2012

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DEDICATION

This dissertation is dedicated to my family and friends. My mother, you demonstrated by example throughout my life that nothing is impossible and there is no incident too severe

for which you allow the smile to be removed your face and strength from your heart. Without seeing this first-hand Mom, I don't believe I could have succeeded. You are my inspiration. My father, you have always been there for your little girl. Thank you for my second chance at life. I am blessed to have you both as parents. To all my friends who have walked beside me throughout the good and bad, I thank you all for your support.

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v

Tatiana Trejos, Howard Holness, Mimy Young, Wen Fan, Maria Perez, Steve Wise, Ben Naes and Monica Joshi. You have all enlightened my life. Please forgive me if I have failed to list anyone.

ABSTRACT OF THE DISSERTATION THE DISCRIMINATION AND ASSOCIATION OF FLOAT GLASS AND THE QUANTITATIVE ANALYSIS OF LIQUIDS FROM AEROSOLS AND MICRODROPS USING LASER INDUCED BREAKDOWN SPECTROSCOPY

by

Erica M. Cahoon

Florida International University, 2012

Miami, Florida

Professor José Almirall, Major Professor

Glass is a common form of trace evidence found at many scenes of crimes in the form of small fragments. These glass fragments can transfer to surrounding objects and/or persons and may provide forensic investigators valuable information to link a suspect to the scene of a crime. Since the elemental composition of different glass sources can be very similar, a highly discriminating technique is required to distinguish between fragments that have originated from different sources.

The research presented here demonstrates that Laser Induced Breakdown Spectroscopy (LIBS) is a viable analytical technique for the association and discrimination of glass fragments. The first part of this research describes the optimization of the LIBS experiments including the use of different laser wavelengths to investigate laser-material interaction. The use of a 266 nm excitation laser provided the best analytical figures of merit with minimal damage to the sample. The resulting analytical figures of merit are presented. The second part of this research evaluated the sensitivity of LIBS to associate or discriminate float glass samples originating from the same manufacturing plants and produced at approximately the same time period. Two different sample sets were analyzed ranging in manufacturing dates from days to years apart. Eighteen (18) atomic emission lines corresponding to the elements Sr, K, Fe, Ca, Al, Ba, Na, Mg and Ti, were chosen because of their detection above the method detection limits and for presenting differences between the samples. Ten elemental ratios producing the most discrimination were selected for each set. When all the ratios are combined in a comparison, 99% of the possible pairs were discriminated using the optimized LIBS method generating typical analytical precisions of ~5% RSD.

The final study consisted of the development of a new approach for the use of LIBS as a quantitative analysis of ultra-low volume solution analysis using aerosols and microdrops. Laser induced breakdown spectroscopy demonstrated to be an effective technique for the analysis of as low as 90 pL for microdrop LIBS with 1 pg absolute LOD and 20 μ L for aerosol LIBS with an absolute LOD of ~100 fg.

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LIST OF ABBREVIATIONS

LIBS	Laser Induced Breakdown Spectroscopy
SP	Single-pulse
DP	Double-pulse
ICP-MS	Inductively Coupled Plasma Mass Spectrometry
LA	Laser Ablation
LA-ICP-MS	Laser Ablation Inductively Coupled Plasma Mass Spectrometry
μXRF	Micro X-ray Fluorescence
SEM-EDS	Scanning Electron Microscopy Energy Dispersive Spectroscopy
WDS	Wavelength Dispersive Spectroscopy
AAS	Atomic Absorption Spectroscopy
NAA	Neutron Activation Analysis
NIST	National Institute of Standards and Technology
ASTM	American Society of Testing and Materials
FIU	Florida International University
CRM	Certified Reference Material
Nd:YAG	Neodymium: Yttrium Aluminum Garnet
FWHM	Full Width Half Maximum
LTE	Local Thermodynamic Equilibrium
ppm	Parts Per Million
UV	Ultraviolet
IR	Infrared
SD	Standard Deviation

- RSD Relative Standard Deviation
- LTSD Lens-To-Sample Distance
- CCD Charge Coupled Device
- LOD Limit of Detection

1 Introduction: Research Motivation

Glass is a commonly encountered type of trace evidence found at many crime scenes. Glass fragments may provide the forensic investigator with valuable information. The fragments are often produced by breaking a window during a forced entry or as a result of the high forces to vehicle windows during a hit-and-run accident or other collisions. These glass fragments may then be transferred to all surrounding objects and persons and may provide forensic investigators valuable information of association to link a suspect to the scene of a crime. If the glass was broken during a crime act, these glass fragments could potentially be used as evidence, associating an individual to the event.

Since the elemental profile of glass can be very similar, a highly discriminating technique is required to distinguish between fragments that have originated from different sources. Historically, the forensic analyses of glass fragments have been based on the comparison of color, density, thickness, transparency and refractive index. As a result of the lack of discrimination power of these analytical techniques, a need developed for more sensitive, complementary instrumentation for the forensic analysis of glass fragments. For instance, refractive index was the method of choice for many forensic laboratories, however, glass manufacturers now target specific optical properties in glass, creating a narrow range of refractive indices ¹. As a result, elemental analysis has been suggested as an additional technique ^{2,3}. With use of more sensitive analytical techniques, the forensic analyst may associate or discriminate, with a high degree of certainty, between the glass fragments in question to those of known origin. These associations may establish a connection between the suspect and scene of the crime.

Varying concentrations in float glass may allow glass to be chemically characterized to its source. If the variation in elemental composition of float glass is greater between sources than within sources, this variation allows for the forensic discrimination of glass. Certain elements are controlled in the glass manufacturing process to obtain specific properties for the end-use product. The major elements which are controlled may provide discrimination ⁴. However, it is predominantly the minor, trace and the impurities that provide the forensic investigator the ability to discriminate or associate glass samples ⁵.

Although LIBS is more commonly used for analysis of solid matrices, solution analysis is investigated in this research. Solutions provide the analyst a homogeneous sample that can incorporate internal standards and are easily matrix-matched. Most sampling volume requirements are approximately a milliliter or more for the wellestablished techniques of inductively coupled plasma mass spectrometry (ICP-MS) or ICP-optical emission spectrometry (ICP-OES)^{6,7}. Very small volumes, i.e., picoliters to microliters, present a considerable challenge when measuring very low concentrations of trace metals.

My research describes the development and validation of the use of Laser Induced Breakdown Spectroscopy as an analytical technique for the association and discrimination of forensic glass and for ultra-low volume analysis of aerosols and, for the first time, microdrops delivered in an ambient atmosphere.

1.1 Significance of Study

Laser induced breakdown spectroscopy will be presented as an analytical tool for the forensic association and discrimination of float glass by elemental profiling. Secondly, LIBS will be presented as a tool for the quantitative analysis of small volumes from aerosols and, for the first time, microdrops.

Float glass is a commonly encountered type of evidence for the forensic investigator. The similar elemental composition of float glass requires techniques with high analytical sensitivity and reproducibility so the forensic analyst may achieve accuracy and discrimination. The use of elemental analysis for the forensic glass comparisons is not a recent development. It dates back to as early as 1973 with the use of neutron activation analysis (NAA) ⁸ to distinguish glass from different sources. Currently, forensic laboratories perform elemental profiling of glass predominantly using micro x-ray fluorescence (μXRF), ICP-MS and laser ablation-ICP-MS (LA-ICP-MS).

The mature techniques of μ XRF, ICP-MS and LA-ICP-MS are advantageous; however each method has limitations. Minor and trace elements present in low concentrations are problematic for μ XRF as they lie below the analytical limits of detection (LOD). Milligrams of sample are required for the necessary repeated analysis with ICP-MS^{7,9-11}, which may be unmanageable when only small fragments are transferred during a crime. The invention of laser ablation for sample introduction into the ICP-MS has simplified the analysis of solids, such as float glass, and is now regarded as the "gold standard" for discrimination between similar elemental profiles of glass samples originating from different sources, or to determine the association from the same source^{3,12-15}. Despite the excellent analytical performance of LA-ICP-MS, this

instrumentation is complex, expensive and is not available for many forensic laboratories. Without forensic laboratories having access to sensitive analytical techniques, a need is created to develop a less expensive and robust method that can be used for the chemical characterization of trace evidence, such as float glass, that is commonly encountered in the forensic laboratory.

The studies that are presented throughout this manuscript demonstrate the utility of LIBS as an alternative analytical technique for the forensic analysis of glass. The research in the chapters to follow describes method development and validation for LIBS as an analytical technique for the forensic analysis of glass. The optimization of laser energy, gate delay, integration times and laser irradiance to improve crater morphology, all for improving reproducibility, limits of detection, precision and accuracy are discussed. The discrimination capabilities of LIBS will be evaluated by two float glass sample sets: 1) consisting of 49 colorless float glass samples manufactured in a single plant from May 1997 to September 2001 and 2) consisting of 27 colorless float glass samples collected from September 2008 to April 2010 from a different single manufacturing plant, both sets range in manufacturing date from days to years apart. On the basis of LIBS still being a forthcoming technique, the results produced are compared to LA-ICP-MS. LA-ICP-MS is also evaluated on the percent discrimination achieved for float glass sample set two.

The final study consists of developing an analytical method to demonstrate the analytical capabilities of LIBS as a technique for the quantification of low volume solution analysis with aerosols and microdrops. Employing LIBS as an analytical technique for solutions, eliminates certain disadvantages observed with LIBS liquid

analyses, such as splashing, while also eliminating the greater volume requirements needed for solution sampling by techniques such as ICP-MS or ICP-OES.

1.2 The Glass Matrix

The American Society of Testing and Materials (ASTM) defines glass "...as an inorganic product of fusion which has been cooled to a rigid condition with crystallization..."¹⁶. Common raw materials for float glass manufacture consist of silica (SiO₂) that is responsible for the high transition temperature of glass and sodium carbonate which lowers the transition temperature. Other ingredients added are dolomite, calcium carbonate, magnesium oxide, sodium oxide and aluminum oxide, as they adjust chemical and physical properties in glass ¹⁷.

Glass is usually classified into three groups by its chemical composition: 1) soda lime glass, 2) lead glass and 3) borosilicate glass. These three types account for 95% of all glass, with soda lime glass being 72% silica, it constitutes for approximately 90% of manufactured glass ¹⁸. Bottles, jars, architectural and automobile glass are examples of soda-lime glass. The many applications of soda-lime glass is a result of its physical and chemical properties, with light transmission being the most significant¹⁹. The smooth, non-porous surface allows for bottles to be easily cleaned, to be filled with beverages with no affect to flavor and with no harmful substances. Lead glass, the second group, is produced by replacing much of the lime with lead oxide. Lead glass exhibits high refractive index, which are used most as decorative glass, i.e., vases or bowls. Borosilicate, the third group, is resistant to chemical corrosion and temperature change as

a result of the high SiO_2 in the glass¹⁹. Borosilicate glass is commonly used in the chemical laboratory.

The manufacturing of float glass consists of mixing the batch (raw material) with crushed cullet (recycled glass). The melting furnace is made of refractory bricks and heated to approximately 2900° F. The furnace has a capacity to contain as much as 2000 kg of raw materials, see Figure 1. The glass then leaves the furnace at a temperature of approximately 1900° F and is fed into a bath of molten tin.



Figure 1. The float glass furnace at Pilkington North American Inc., Stockton, CA



Figure 2. Float glass being pulled onto rollers at Pilkington North American Inc., Stockton, CA

Tin is appropriate for the float glass process as a result of the high specific gravity of tin and its immiscibility into the molten glass. The tin bath is kept in a controlled atmosphere of hydrogen and nitrogen to prevent oxidation. The glass spreads out flat and smooth on the molten tin. The thickness of the glass is controlled by the pull of a ribbon, see Figure 2. The two photographs above, Figure 1 and 2 were provided by my mentor, Dr. Almirall.

The temperature is gradually decreased to approximately 1000° F in the annealing lehr, where the glass sheet can be placed on the rollers. The glass in then cut to a predetermined sizes ^{18,20,21}. Figure 3 illustrates the different processes for the manufacture of float glass ²¹. The standard specifications for float glass have been established in method ASTM C 1036 Standard Specification for Flat Glass.



Figure 3. Schematic of the float glass manufacturing process²¹

There are approximately 40 float glass plants in the United States corresponding to eight manufacturers: Cardinal Glass Industries, Guardian Industries Corporation, AFG Industries, Inc., ACH Float Glass Operations, Pilkington North American, Inc., PPG Industries, Inc., Saint-Gobain Glass, and Vitro America, Inc. These plants are designed to operate seven days a week, 365 days a year for ten years or more, typically producing between 300-600 tons of glass per day ²¹. The lifetime of the furnace is approximately 10 years as a result of the corrosion of the refractory bricks¹⁹. It is the process of this corrosion that causes differences in the trace elemental composition. It is these trace elements that provide the greatest discrimination between different sources and dates of manufacture between glasses.

Float glass manufacturing plants, Cardinal Glass Industries and Pilkington North America, Inc., provided float glass samples for this research.

1.3 Elemental Analysis of Glass

Numerous elemental analysis techniques have been employed for the discrimination and chemical characterization of glass. These techniques include spark source mass spectrometry²², atomic emission spectroscopy (AES)²³, atomic absorption spectroscopy (AAS)², x-ray fluorescence (XRF)^{2,23,24}, neutron activation analysis (NAA)⁸, scanning electron microscopy (SEM) coupled to both energy dispersive spectroscopy (EDS) and wavelength dispersive spectroscopy (WDS)²⁴⁻²⁶, particle induced x-ray emission (PIXE)²⁵, inductively coupled plasma atomic emission spectrometry (ICP-AES)^{2,23,25}, inductively coupled plasma mass spectrometry (ICP-MS) ^{11,23,27}, laser ablation inductively coupled plasma mass optical emission spectrometry (LA-ICP-OES)²⁷, laser ablation-ICP-MS (LA-ICP-MS)^{3,12-15} and LIBS^{3,13,28-31}.

The potential to discriminate glass was documented with NAA, as early as 1973⁸. Samples analyzed by NAA are bombarded with neutrons, causing the elements to form radioisotopes. Different radioisotopes have different half-lives and these radioactive decay paths for each element are well known. The radioactive emissions are counted, providing the analyst with the elemental composition. Coleman *et al.*⁸ analyzed 25 elements from window glass originating from England and Wales using neutron activation analysis. The authors demonstrated that the frequency distributions of the elemental concentrations could be used for the forensic comparison of glass.

Scanning electron microscopy uses a focused beam of high-energy electrons causing the emission of X-rays. X-ray fluorescence spectrometry relies upon the measurement of characteristic X-rays produced by an X-ray source. X-ray radiation is produced by when an inner electron of the atom is displaced by either the high-energy electron beam or X-ray beam. Electrons in higher energy states relax to fill the lower energy states. The energy difference between the two electronic states is given off as Xrays. The intensities of these X-rays are proportional to the elemental concentration, providing qualitative and quantitative information. For the discrimination among different glass sources, SEM and XRF report the use of elemental ratios for the intensities in glass^{24,26}. Dudley *et al.* in 1980 used XRF and 10 elemental ratios with Ca for determining the elemental concentrations in 50 pairs of window and non-window glasses having indistinguishable refractive indices. The elemental ratios discriminated 95% of the glass samples. Ryland correctly classified 93% of sheet and container glass using a μ XRF comparing the Ca/Fe ratio²⁶. He reported that a high Ca/Fe ratio is indicative of container glass or tableware while a low Ca/Fe ratio is representative of sheet glass. Advantages of XRF are that it is a non-destructive technique with little interferences from spectral lines. Disadvantages are high limits of detection (~100 ppm) and glass fragments are often irregularly shaped, affecting take-off angles and causing poor precision and accuracy.

The inductively coupled plasma may either be coupled with an optical emission spectrometer or a mass spectrometer. The inductively coupled plasma is a radiofrequency-induced plasma from an induction coil to produce a magnetic field. When coupled to an optical emission spectrometer, the light is separated according to its wavelength and the intensities are characteristic of the elemental concentration. The mass spectrometer separates ions according to their mass-to-charge ratio. These detectors are very sensitive while also quantitative. Both these methods require the samples to be in solution. The dissolution of glass requires an elaborate method. The ASTM provides a protocol for the dissolution and analysis of glass by ICP-OES³². ICP-OES is a

destructive technique where the glass fragments need to be crushed and digested in a combination of HF, HNO₃ and HCl. The glass and acid mixture are then heated till dissolution of the glass.

Hickman was the first to propose a classification procedure for container, sheet, tableware or headlamp glass using ICP-OES^{33,34}. He analyzed manganese (Mn), iron (Fe), magnesium (Mg), aluminum (Al) and barium (Ba) with refractive index and was able to discriminate 91% of 349 glass samples. Hickman later expanded the elemental menu to include; strontium (Sr), Fe, arsenic (As), cerium (Ce), cobalt (Co), cesium (Cs), lithium (Li), rubidium (Rb), antimony (Sb) and lead (Pb), to provide higher discrimination³⁴⁻³⁶. Koons et al. compared 182 sheet and container glasses by ICP-OES⁹ using Al, Ba, Mg, Fe, Sr, Mn, Ca, Na and Ti. He classified all samples correctly except for two container glasses from the same manufacturing plant classified as sheet glass and two sheet glasses classified as container glass. Koons et al. classified 180 of the 184 samples using principal component analysis (PCA) and cluster analysis⁹. This study concluded that elemental composition can classify glass samples from the same manufacturer, thereby suggesting that the elemental profile can provide good evidence of an association between the manufacturer and the glass fragment. Parouchais et al.³⁷ used ICP-MS to analyze 62 elements within glass. To decrease physical, spectral and chemical interferences that may arise from the dissolution of glass, the authors reported using elemental ratios to discriminate between samples found indistinguishable by refractive index. Suzuki et al.¹⁰ used pairwise comparison of the elements Co, Rb, Sr, Zr, Ba, La and Ce to discriminate 22 windshield float glass samples. The authors reported 100% discrimination using elemental composition and 94% discrimination with refractive

index. With a change in the elemental menu, Zr, Ba, Sb, Sr, Hf, As, Mo and Pb, Suzuki *et al.*³⁸ were able to distinguish between all 17 samples (138 pairs) of headlight glass with ICP-MS and only 19 pairs with refractive index.

In 1985, Gray³⁹ developed laser ablation (LA) as a new sample introduction system for ICP-MS. This introduction generates particles when the laser interacts with the solid sample. These particles are then swept into the ICP-MS with a carrier gas. Laser ablation eliminated the laborious and time consuming solid sample preparation, while providing the same sensitive technique. Laser ablation brought about several advantages; practically no sample preparation, no contamination from chemicals, less interferences as a result of no solvents and spatial resolution. A more in-depth explanation of LA-ICP-MS will be provided in the next section.

To validate LA-ICP-MS, it was compared to the mature technique of ICP-MS. Individual studies were done demonstrating that LA-ICP-MS provided equally as good figure of merits (precision, bias, and limit of detection)^{12,40,41}. Trejos *et al.*⁴¹ conducted micro-homogeneity study to evaluate the elemental composition of glass samples found at crime scenes. The results demonstrated that float glass is homogeneous at the microanalysis level, allowing LA-ICP-MS to be viable technique for the forensic analysis of float glass. Inherent heterogeneity was observed with headlamps and container glass. The authors recommended sampling at many different locations to correctly characterize the elemental profile. An inter-laboratory cross validation study was conducted to verify different laser ablation systems with different ICP-MS instrumentation. The objective was to compare inter-laboratory results for similarity in efforts to improve analytical protocol¹⁴. It was determined that many different laboratories were able to produce standard deviation of less than 10% for most all elements.

Laser induced breakdown spectroscopy is an emerging atomic emission technique for the forensic analysis of glass. The current history of LIBS for the elemental analysis of glass is limited, as no standard protocols currently exist. The LIBS research conducted to date has been successful in the forensic analysis of glass^{3,13,28,42}. Naes *et al.*³ demonstrated that LIBS produces the same 99% discrimination, with no false exclusions, as µXRF and LA-ICP-MS with a different element menu of automobile float glass ³. Naes *et al.* found the 10 most discriminating elemental ratios to be Al/Na, K/Ca, Al/Fe, Fe/K, Ca/K, Fe/Al, K/Ca, Al/Sr, Sr/K and Na/K. Bridge *et al.* achieved an 83% and 74% discrimination of automobile float glass with LIBS, however when combined with refractive index measurements, the discrimination increased to 99% discrimination for both sample sets, but these authors did not conduct type I and type II error studies ^{13,42}. The precision obtained from both authors were in agreement, Naes *et al.* state the precision is less than 10% RSD and Bridge *et al.* state an average precision of 7% RSD.

LIBS offers a sensitive and fast approach to elemental analysis and permits small sample size with good precision, similar to LA-ICP-MS. LIBS is fairly inexpensive when compared to the more established techniques of LA-ICP-MS, LA-ICP-OES and μ XRF. LIBS is less complex, generates data virtually instantaneously, has the capability to be portable, while providing high sample throughput.

The present section summarizes the advancements that have been made for the elemental analysis of glass by many different techniques. The recent developments in LIBS, has shown it to be a promising technique for the forensic analysis of glass. The

research studies to follow will demonstrate that LIBS is indeed a viable alternative to the expensive instrumentation of LA-ICP-MS for the forensic analysis of glass and should be given consideration in the forensic laboratory.

1.4 Sample Preparation of Solutions and Solid Samples for Chemical Analysis Laser Induced Breakdown Spectroscopy is predominantly a solid sampling technique that has been demonstrated to compete favorably with μ XRF-EDS and LA-ICP-MS^{43,44} for the elemental analysis of some solid matrices. Because of its multi-elemental detection, non-destructive nature, minimal sample preparation and in-situ analysis, LIBS has become a very popular analytical technique offering simplicity of operation and data analysis as attractive features.

Analytical chemists use atomic spectroscopy tools for both solution and solid analysis, and laser-based solid sampling tools have been coupled to ICP plasmas. Techniques based on atomic spectroscopy are important in trace analysis of solutions but many solution techniques suffer from labor intensive and time-consuming sample preparation. Solutions provide homogeneous samples that can incorporate internal standards and external calibration methods can be easily developed but require sample preparation (sample dissolution) when the sample is in solid form. Direct solid sampling may also require sample preparation, primarily to homogenize the sample prior to analysis by pelletizing a powder sample, for example. The sample is milled into a homogeneous powder and then pressed into a pellet ideally producing a flat, homogeneous surface. In an effort to improve precision and decrease elemental fractionation, particle size effects have been investigated. It has been reported that, smaller particle sizes produce enhanced ionization in the plasma in the LA-ICP-MS experiment⁴⁵⁻⁴⁷. Arroyo *et al.* found that reducing the particle size to less than 1 µm allowed for representative sampling and improved precision on soil samples⁴⁷.

Homogeneity is essential in laser micro-sampling techniques, i.e., LIBS and LA-ICP-MS, where only tens to hundreds of nanograms to micrograms of material are removed for analysis. Many factors pose challenges during solid sampling, such as sample size, shape, heterogeneity and the lack of matrix-matched standards. Without adequate sample size, one may not be able to complete the necessary repeated measurements needed to perform statistical analysis and adequately assess sample heterogeneity. Solid sampling quantification is challenging when matrix-matched standards are not readily available and normally requiring the analyst to produce a matrix-matched standard.

It is common for liquid sampling volume requirements to reach up to a milliliter or more for repeated measurements of the sample for well-established techniques ICP-MS and ICP-OES^{48,49}. The measurement of very low concentrations of trace metals contained in very small volumes presents a considerable challenge to the analytical chemist.

Quantitative analysis of liquid samples by LIBS has posed to be rather challenging because, in part, the following inherent drawbacks. In liquids, the plasma radiation is weak because of the quenching by the water and weakening and broadening of the spectral lines as a result of collisions and the Stark effect⁵⁰. Splashing from direct analysis of liquid surfaces may contribute to the extinction of plasma emissions, thereby resulting in shorter plasma lifetimes. The produced shockwaves increase the shot-to-shot variation, while splashing and the formation of bubbles created inside the liquid may produce quenching and change the characteristics of the plasma, thereby suppressing the LIBS signal⁵¹. Trying to reconcile for these disadvantages, different methods have been

proposed including initiating the plasma within the liquid bulk of the sample to reduce splashing, however the plasma lifetime was extremely short under these conditions, approximately 1 µs or less⁵². Other approaches for minimizing the drawbacks include the use of laminar flows⁵², jets^{53,54}, freezing the samples in ice⁵⁵, LIBS within cavitation bubbles⁵⁶, double-pulse plasma generation^{50,57}, and converting liquid solutions into a solid matrix⁵⁸. Previous research by Neimax⁵⁹, Hanh⁶⁰ and Jantzen⁶¹ have demonstrated that LIBS is capable of microdrop analysis.

The focus of the current research is to incorporate both aerosol analysis and for the first time, the use of microdrop printing in ambient conditions, to generate small droplets that can be entrained in a double-pulse LIBS plasma.

Continuous mode inkjet printing will be used to deliver microdrops containing ~90 picoliter volumes for LIBS analysis. Inkjet printing is a contactless method for depositing precise volumes of solutions and able to deliver drops ranging from a few microns in diameter to tenths of a millimeter⁶², depending on the nozzle orifice. Section 1.8 will present further details regarding microdrop printing.

The motivation of this research is to use LIBS to accurately and precisely analyze small volumes of solution, $\leq 300 \ \mu$ L for aerosol analysis and 90 pL for singlemicrodrops. These two methods eliminate the splashing and the sample preparation steps that were needed in the above discussed LIBS solution methods, as well as dramatically reduce the total volume needed for analysis.

It has been noted that conventional single-pulse LIBS is less sensitive than the competing atomic spectroscopic technique of ICP-OES that utilizes a sustained plasma as the excitation source but also requires much more analytical volume. In an effort to
increase the LIBS sensitivity, double-pulse LIBS excitation will be explored. Different laser pulse configurations have contributed to improving the limits of detection (LOD), by increasing the LIBS signal^{63,64}. These techniques use a combination of two lasers or two pulses from one laser. Both are spatially overlapped and the two laser pulses are focused and separated some nanoseconds to tens of microseconds and will be discussed in sections that follow.

1.5 Physics of Laser Ablation

In principle, there are no sample size requirements and any type of solid sample can be ablated. Laser ablation requires almost no sample preparation thereby eliminating contamination issues that arise with chemical dissolution, required by some methods. Solution analysis requires approximately a few milligrams of sample that is needed for the digestion and a total volume of approximately milliliters of sample. Laser ablation removes nanograms to microgram quantities of mass, making the sampling technique virtually non-destructive. The laser ablation process for LIBS and LA-ICP-MS are identical, however optimized parameters for each system will vary as will the equipment required and detection capabilities. Laser ablation is becoming the leading technology for the chemical analysis of solid samples⁶⁵.

Laser ablation has been defined by the processes of material melting, fusion, sublimation, erosion and explosion. Laser ablation is an involved process, the lasermaterial interaction causes mass to leave the surface in the form of ions, electrons, atoms, molecules, clusters and particles, with each of these processes separated in time and space⁶⁶.

The three main processes for laser ablation are: 1) bond breaking and plasma ignition, 2) plasma expansion and cooling and 3) particle ejection and condensation⁶⁷. The time period for these processes varies by orders of magnitude with electron absorption of the laser energy occurring at 10⁻¹⁵ seconds, to particle condensation occurring 10⁻³ seconds after completion of laser pulse. Figure 4 demonstrates these processes and corresponding mechanisms. The laser irradiance, pulse duration, thermal

and optical properties of the sample material are critical properties and influence these processes.



Figure 4. The time scale of events from laser pulse to particle ejection⁶⁸

The dominant mechanism is thermal vaporization for a nanosecond laser pulse with irradiances less than 10^8 W/cm². The temperature increases causing a transition from solid to liquid, liquid to vapor and vapor to plasma. The electron emission starts in the picosecond time frame, before the completion of the nanosecond laser pulse. Inverse Bremsstrahlung is dominant as the electrons emitted will gain energy from the incoming laser pulse through the collisions with the ionized vapor mass leaving the sample surface⁶⁹. When the kinetic energy of the electrons in the plume is higher than the ionization potential of the vaporized atoms, the plume may absorb the tailing end of the laser energy and partially shield the sample surface from further laser ablation⁷⁰.

Picosecond laser pulse widths exhibit thermal and non-thermal mechanisms, such as Coulomb explosion, with irradiances between 10^{10} - 10^{13} W/cm². Femtosecond pulses

with irradiances greater than 10^{13} W/cm², Coulomb explosion is the dominant process⁶⁷ in plasma formation.

Plasma shielding influences the amount of mass that is ablated into the LIBS plasma. In nanoseconds, the plasma will develop significantly. With a laser pulse width of less than 1 nanosecond, the absorption of laser energy into the developed plasma may be negligible. The picosecond width may partially be absorbed by an air plasma formed during the early stage electronic plasma⁷¹. The femtosecond pulse widths are neglected as a result of the pulse being too short to be absorbed by the plasma.

The electron density, electron temperature and the plasma expansion speed are highly dependent on the laser properties. The initial mass, energy and gas environment that the plasma is developed in will influence the expansion. These high laser energies cause the sample to transition rapidly from super-heated liquid to an explosion of vapor and liquid droplets.

When the absorbed laser energy is sufficient to fulfill latent heat of melting and vaporization, there is transfer of mass from solid into the plasma⁶⁸. When the sample surface approaches a temperature several times the vaporization temperature, the laser energy can then significantly transfer more mass into the vapor phase. From this point the particles may then be swept into the ICP-MS. For LIBS analysis, an adiabatic plasma exists for approximately 1 microsecond where inverse Bremsstrahlung is the dominant factor, after this occurrence, the spectral line radiation is apparent for LIBS.

1.6 Introduction to Laser Induced Breakdown Spectroscopy

Laser induced breakdown spectroscopy is an emerging method of atomic emission spectroscopy. A generalized LIBS setup requires: a pulsed laser, mirror, focusing and collection optics for the emitted radiation, and an optical fiber coupled to a spectrometer, see Figure 5.



Figure 5. Single-pulse and double-pulse LIBS schematic

LIBS utilizes a high-powered laser pulse focused by a lens to a sub-millimeter spot on or in the solid, liquid or gaseous sample. A laser pulse of sufficient energy comes into contact with the sample surface that ablates a microgram or less quantity of material. The atomic and molecular structure of the sample is broken down inducing vaporization. The ablated material forms a plasma, in the form of molecules, neutral atoms, excited atoms, ions and electrons, which expands at a velocity much faster than the speed of sound, producing a shock wave in the surrounding atmosphere. Throughout this process there is a background continuum that decays more quickly with time than the spectral lines. The continuum is primarily the result of bremsstrahlung process in which photons emitted by the electrons is the dominating process ⁷². During the following microseconds the plasma will decay through radiative quenching and electron-ion recombination processes ⁷². Figure 6 demonstrates the timeline from laser pulse emission of spectral lines. It is usually at the microsecond time frame that the emission light is collected, transferred and detected. Each element has an exclusive emission spectrum; the wavelength corresponding to the emission line.





LIBS typically removes nanogram to microgram quantities of mass ³¹, classifying it as a surface technique. However, multiple pulses at the same location can be used to ablate the surface, thereby removing surface contamination and exposing underlying layers. The ablated mass is characteristic of the original sample, allowing the analyst to "fingerprint" the species. Each firing of the laser will produce a LIBS spectrum. The analytical signal is calculated by the integration of the emission line intensity or peak area. Typically, LIBS measurements are averaged or accumulated to increase precision and accuracy, and to average out signal variance.

1.6.1 Development of LIBS

Research began by spectroscopists with the invention of the laser in 1960 by Maiman⁷³. The first LIBS plasma was reported by Brech and Cross⁷⁴, where a laser was used to produce a plasma in 1962. Debras-Guedon and Liodec reported the first analytical use of LIBS on surfaces in 1963⁷⁵. Shortly, proceeding the analytical accomplishment of LIBS on surfaces, the first instrument was produced based on the LIBS technique⁷⁶. An auxiliary spark discharge was used to produce the light for spectral analysis. However, as a result of the poor accuracy and precision produced, this technique did not become very popular. During these early years the laser was predominantly used as an ablation source into a conventional plasma source. The detector used in the 1960s to produce temporally resolved spectra were commonly the streak camera and rotating mirrors, until 1971 when Schroeder *et al.* developed a system to electronically gate and average the plasma signals⁷⁷. However, it was not until the 1980's that a renewed interest was developed in spectrochemical analysis by LIBS. This renewed interest of LIBS was contributed to the advances in instrumentation as the laser and other components of the LIBS system became smaller, the advantages became more apparent.

Laser induced breakdown spectroscopy has been referred to as laser induced breakdown plasma spectroscopy (LIPS) or laser spark spectroscopy (LSS). Over the last two decades LIBS has developed rapidly. Pioneers in LIBS research were the scientists at

Los Alamos National Laboratory. They demonstrated in the early 1980s that LIBS was able to detect hazardous gases and vapors in air⁷⁸ and small amounts of beryllium in air and on filters^{79,80}. Proceeding from the research of the Los Alamos National Laboratory, many more LIBS applications were reported; liquids were analyzed at surface or in bulk^{81,82}, salt concentration was measured in sea droplets⁸³ and carbon content in steel ⁸⁴ to list a few. With the new developments in lasers and detection devices, new applications have focused on practical problems, such as real-time monitoring of toxic metal emissions⁸⁵, quality assessment of steal⁸⁶ and for planetary exploration the LIBS rover was developed by NASA ⁸⁷. In efforts to make LIBS more quantitative, many scientists have explored the fundamentals of LIBS, such as plasma fundamentals and laser ablation. These topics will be covered in the upcoming sections.

There has been considerable growth within the LIBS community since the development in the 1960's as LIBS has advanced in laboratories throughout the world. For instance, less than 50 papers were published per year from 1965 through 1990. However, there was a dramatic increase in LIBS publications from 2000 to 2005 with over 200 papers being published⁸¹. Currently, LIBS papers are appearing in prominent journals every month.

Commercial LIBS instruments are being manufactured by companies such as, Applied Spectra, Foster and Freeman, Applied Photonics and Photon Machines. These commercial LIBS systems have been purchased by analytical and forensic laboratories. The LIBS community has grown and developed international and national scientific conferences dedicated solely for the purpose of being able to exchange information and observe the contributions of other LIBS scientific research.

1.6.1 LIBS Plasma Fundamentals

A plasma, the fourth state of matter, is composed of atoms, ions and free electrons and is overall electrically neutral. One of the main parameters for characterizing a plasma is the degree of ionization. The LIBS plasmas are typically weakly ionized as the ratio of electrons to other species is less than 10%⁸¹. Hughes⁸⁸ described two steps leading to breakdown threshold of the matrix as a result of optical excitation. First, a few free electrons serve as receptors to the laser energy, producing collisions with photons and neutrals. The second step is the background continuum. With a laser irradiance beyond 10^9 W/cm² with a nanosecond or shorter laser pulse, an explosion occurs⁶⁸. The sample surface rapidly heats, melts and vaporizes material as a result of the laser-material interaction with the leading edge of the laser pulse. As the energies of the electrons grow, ionization is produced through collisions, other electrons and energy absorption. The Bremsstrahlung process is a result of photons being emitted by electrons that are accelerated or decelerated in collisions. Recombination happens when a free electron is captured into an atomic or ionic energy level and the excess kinetic energy is released in the form of a photon. The continuum is a result of Bremsstrahlung and recombination events.

The laser induced plasma will continue to expand after the end of the laser pulse. The expansion of the plasma is dependent upon the amount of mass ablated, the energy and spot size of the laser and the surrounding environment.

The plasma expands outward from the focal volume with an initial rate of expansion on the order of 10^5 m/s, the ablated mass compresses and a shock wave is produced that is audible to the analyst⁷². The early plasma expansion from a nanosecond

laser on a float glass sample can be seen in Figure 7. This is a shadowgraph taken within the laboratory demonstrating the growth of the shock wave from 880 ns to $1.15 \,\mu$ s.



Figure 7. Shadowgraph demonstrating shockwave growth from 880 ns to 1.15 μ s When the pressure of the plasma plume equals the ambient pressure, the plasma expansion will stop.

The plasma evolves through many transient states from initiation to extinction. LIBS requires time resolution to avoid collection of the continuum and for the collection of light during the period that the analyte signal of interest is dominant. As the laser induced plasma cools, photons characteristic of the elemental composition of the sample surface are emitted. Neutrals are formed by the recombination of ions and electrons and other species recombine to form molecules as demonstrated in Figure 6.

Plasmas are diagnosed by their properties, such as plasma temperature and electron density, as well as their spectral lines. The spectral line intensities are dependent on the environment of the emitting atom. Lines are characterized by their wavelength, intensity and shape that are directly related to the density of the plasma and the electronic temperature. There are different broadening mechanisms for the spectral lines.

Natural broadening is a result of the excited states lifetime, which results in a Lorentzian profile. Doppler broadening arises as a result of the random thermal motions of the emitting atoms and results in a Gaussian line shape. However, Doppler broadening is negligible in comparison to the broadening being caused by charged particles. Stark broadening is dominant in LIBS plasmas⁸⁹ because of the high electron densities, i.e., $\sim 10^{15}$ - 10^{18} cm⁻³. Stark broadening is the interaction between the atom and the electric field, as the atom interacts with fast moving electrons and slow moving ions producing a Lorentz shape. This results in the line profiles being dominated by Stark broadening for the considerable time period⁷⁰.

The intensity of spectral lines is dependent of the transition probability and on the excitation conditions. When the electron impact excitation of atoms is high, as in a LIBS plasma, the population of the excited states is in agreement with the electron temperature. Electron temperature is based on the assumption that local equilibrium exists. The LIBS plasmas are described by local thermodynamic equilibrium (LTE). For LTE to exist to collisional processes must be more dominant over the radiative processes. LTE will hold true for high electron density plasmas⁷⁰. When plasmas are in the state of LTE, a temperature can be found using Boltzmann and Saha equation's relationship between excited and ionic states population density⁷⁰. LTE can be assumed if

$$N_e >> 1.6 \times 10^{12} T^{1/2} (E_2 - E_1) \text{ cm}^{-3}$$
 (1)

where N_e is the electron density, T is electron temperature in K, and E_2 - E_1 is the energy difference in electron volts.

Plasma temperature has a high electron density at atmospheric pressure which allows the assumption of LTE and then the use of the Boltzmann and Saha equations⁹⁰. If LTE is assumed then the electron temperature, T_e , can be assumed to be equal to the excitation temperature, T_{exc} ⁹¹. The Boltzmann equation provides relationships between transition line intensities from the same ionization stage and the Saha equation provides relationships between transition line intensities from different ionization stages. Both the Boltzmann plot and Saha-Boltzmann plot have been used by other researchers for the determination of excitation temperature⁹²⁻⁹⁴. The Boltzmann equation is used to determine the plasma temperature:

$$\frac{N_n}{N} = \frac{g_n e^{\frac{-E_n}{kT}}}{\sum_n g_n e^{\frac{-E_n}{kT}}} \equiv \frac{g_n e^{\frac{-E_n}{kT}}}{Z(T)}$$
(2)

where *N* is the total number of atoms or ions per m^3 , N_n , E_n , and g_n are the population density, energy, and statistical weight of the quantum state *n*.

The Saha equation is written as

$$\frac{N_e N^z}{N^{z-1}} = \frac{2Z^z(T)}{Z^{z-1}(T)} \left(\frac{mkT}{2\pi\hbar^2}\right)^{\frac{3}{2}} e^{-\frac{E_{\omega}^{z-1} - \Delta E_{\omega}^{z-1}}{kT}}$$
(3)

The ionization of the species is represented by the superscript, $N_{e_1} E_{\infty}^{z-1}$, and ΔE_{∞}^{z-1} is electron number density, the ionization energy of the species *z*-*1* for isolated systems, and the correction to the ionization potential for interactions in the plasma⁹⁰.

The Saha-Boltzmann expression is similar to the classical Boltzmann expression. Using this method the temperature is determined from the slope of the linear fitting of the plot, which is obtained using several spectral lines from different ionizations, in the same way that the Boltzmann plot provides temperature from only one ionization stage. The Saha-Boltzmann method increases the accuracy of the temperature calculation because it includes the emissivities of lines from different ionic species of the same element⁹⁵. The Saha-Boltzmann equation is defined as

$$\ln\left(\frac{\varepsilon_z \lambda}{Ag_j}\right) = -\frac{1}{kT} E_j^z Z + \ln\left(\frac{hcN^0}{Q^0(T)}\right)$$
(4)

where z indicates the ionic species of the line emissivity, ε . A is the transition probability (s⁻¹), λ the transition wavelength (m), g_j and E_j^z are the static weight (adimensional) and the energy (J) of the upper level of the transition, k the Boltzmann constant, (J K⁻¹) T the plasma temperature (K), h is Planck's constant (J s), c the speed of light (m s⁻¹), N⁰ is the number density of the neutral atoms (cm⁻³) and Q⁰ (T) the partition function for neutral atoms (adimensional). The relationship for equation four is linear. The Saha-Boltzmann equation allows for a linear plot. A line fit to this equation has the slope of -1/kT.

The Stark broadening of lines is a prevailing procedure for determining the electron density, N_e . Stark effects are caused by the electric fields produced by nearby ions and electrons; this is the prevalent cause of pressure broadening in plasmas⁹⁰. Typical plasma densities in the LIBS community range from $10^{16} - 10^{18}$ cm⁻³, and are within the range for Stark broadening to be a dominant mechanism for emission line broadening. The determination of Stark broadening does not require calculating the absolute intensities of the spectral lines, the line shapes and FWHM are sufficient. The spectrum produced by the laser-induced plasma is then fitted to the Lorentzian profile. The Lorentzian function is expressed as

$$y = y_0 + \frac{2A}{\pi} \frac{w}{4(x - x_c)^2 + w^2}$$
(5)

where *w* is the full width half max (FWHM), x_c is the center wavelength, y_0 is the background emission and *A* is the integrated area of the emission line. When the spectral line is fitted to the Lorentzian profile the FWHM is calculated. The FWHM of Stark broadened lines is related to the electron density and can be calculated by the following expression¹⁴

$$\Delta\lambda_{\frac{1}{2}} = 2W\left(\frac{N_e}{10^{16}}\right) + 3.5A\left(\frac{N_e}{10^{16}}\right)^{\frac{1}{4}} \left[1 - \frac{3}{4}N_D^{-\frac{1}{3}}\right]W\left(\frac{N_e}{10^{16}}\right)$$
(6)

where $\Delta \lambda_{\frac{1}{2}}$ (angstroms) is the FWHM, N_e plasma electron density (cm⁻³), A is the ion impact parameter (angstroms), W is the electron impact parameter (angstroms), and N_D is

the number of particles in a Debye sphere and is estimated from the following equation

$$N_D = 1.72 \times 10^9 \, \frac{T^{\frac{3}{2}}}{\sqrt{N_e}} \tag{7}$$

T denotes the temperature in eV. The first term on the right side comes from the electron interaction, while the remaining part of the equation is dependent on the ion interaction. The impact parameters, which correspond to the collisions between two charged particles, have been computed for different line temperatures and can be referenced^{90,96}. It has been demonstrated^{91,96} that the LIBS ion contribution is negligible to the overall broadening and therefore the form of the equation becomes

$$\Delta \lambda_{\frac{1}{2}} = 2W \left(\frac{N_e}{10^{16}} \right) \tag{8}$$

Determination of the electron density by Stark broadening is independent of the assumptions regarding LTE conditions.

Self-absorption will broaden a peak and if severe, the peak will appear flattened. Self-absorption is encountered in high plasma densities when the plasma absorbs its own emission. Self-absorption is caused from resonance lines, when the transition is from the upper state being the lowest excited level to the ground state. Self –reversal occurs as the light passes through the lower temperature regions of the plasma. The spectral lines will potentially look like two lines as a dip forms in the middle. The LIBS measurements usually occur approximately a microsecond after the plasma formation. It is mostly in this time frame that one can assume LTE as the time delay will greatly affect the electron density and the excitation temperature. Electron densities are greater at atmospheric conditions because of the free plasma expansion in air⁷⁰. Typically, when electron densities range from 10^{15} <N_e,< 10^{18} cm⁻³ and excitation temperatures between 0.5<T_e<2 eV, the LTE conditions will be satisfied and both Saha and Boltzmann equations will hold true⁷⁰.

The LIBS spectra are recorded temporally to provide the highest signal-to-noise ratio corresponding to the best precision. Data collections from LIBS experiments were recorded after the laser pulse at a delay of approximately hundreds of nanoseconds to microseconds. Understanding the LIBS plasma expansion during this time period will aid the analyst in producing the optimized parameters for their LIBS measurements.

1.6.2 Double-Pulse LIBS

In addition, to single-pulse LIBS where only one laser is used for ablation and excitation, double-pulse combines two laser pulses. Different laser pulse configurations have contributed to better sensitivity, while gaining signal for LIBS analyses ⁹⁷⁻⁹⁹. These pulses can be the combination of one laser or from two different lasers with an interpulse delay ranging from nanoseconds ¹⁰⁰ to microseconds ⁹⁷. Several double-pulse geometric configuration approaches have been used consisting of either one laser¹⁰¹, or two different lasers¹⁰² to encompass a double-pulse LIBS setup. Geometrical configurations include either collinear, in which the first and subsequent laser pulses are focused to the same location on the sample, or orthogonal. The orthogonal configuration includes one

beam perpendicular to the surface while the other pulse is parallel to the surface.



Figure 8. Schematic of the different double-pulse LIBS configurations: a) collinear, b) reheating orthogonal and c) prespark orthogonal¹⁰³

Within the orthogonal setup there are two configurations: pre-spark and plasma reheat. Pre-spark will pulse the beam parallel to the surface, first creating a spark in air followed by the perpendicular ablation pulse. Plasma reheat will pulse the beam perpendicular for ablation followed by the parallel pulse reheating the plasma. Figure 8, produced by Scaffidi *et al.*¹⁰³, illustrates the different double-pulse LIBS configurations.

The enhancement observed in collinear double-pulse LIBS has been contributed to an increase in mass ablation, plasma volume and the reheating of the plasma by the second pulse ^{99,103,104}. Orthogonal reheat enhancements have been contributed to higher plasma temperatures and electron densities as a result of larger plasma size from the second reheat laser pulse ¹⁰⁵. The enhancements of prespark LIBS are theorized to breakdown the ambient atmosphere prior to the ablation. The breakdown of the ambient

atmosphere results in a larger and faster plasma expansion, while also producing less plasma shielding of the ablation pulse ^{97,105-107}. A more depth study of double-pulse LIBS for the analysis of glass will be covered in the upcoming section.

1.6.3 Optimization of LIBS

The main parameters for optimized performance are laser wavelength, laser pulse energy, lens-to-sample-distance (LTSD), gate delay (time from laser pulse to spectral line detection) and the integration time (time of collection). With optimized parameters, the analyst may improve the LOD, precision and accuracy.

The analytical signal for LIBS is calculated by emission line integrations. If the integrations of the emission line intensities or peak areas vary between replicates during experimentation, the accuracy and precision of the measurement may deteriorate. Optimization of the listed parameters will lessen the shot-to-shot variance, thereby increasing the accuracy and precision.

Laser irradiance is an important parameter to be optimized. It is responsible for the effects caused by laser interaction with the sample and plasma evolution ¹⁰⁸. The sampling process of LIBS is ablation, the interaction of the laser energy with the sample. The ablation is responsible for the amount of mass removed from the sample by the laser pulse. The mass is atomized and ionized by the laser induced plasma from the energy supplied by the laser pulse. The mass in the laser induced plasma is responsible for the LIBS signal observed. Ablating a consistent amount of mass removed will improve precision of the LIBS analytical signal. Laser irradiance will be further discussed in Chapter 2.

The lens-to-sample distance is defined as the depth of focus of the laser. The laser beam is focused at a normal incidence to the sample through a plano-convex lens to a sub-millimeter spot. The sub-millimeter spot may then be focused behind the sample surface. Optimization of the LTSD may increase signal while also producing better precision. It is important to find the optimized position and keep this position constant throughout the experimental measurements for accuracy and precision. It has been documented that adjusting this parameter may aid in the intensity of atomic and ionic emission lines³¹.

The laser induced plasma is a transient process. Time delays are important to monitor the plasma evolution. Ionization is high during the early plasma formation. During the plasma evolution the temporal gating is controlled to avoid the continuum and to capture the spectral emission lines, see Figure 6⁷².

Time resolved spectral detection is an important factor in achieving optimization as it has been demonstrated to enhance sensitivity ¹⁰⁹. Since the plasma evolution from continuum radiation to characteristic radiation has a lifetime of approximately 10 µs, temporally gating the detector and controlling the gate width allows the LIBS operator to view the plasma at a distinct time for a finite integration. Gating the spectrometer is important not to damage the intensified CCD array and will aid in reducing inferences, such as overlapping emission wavelengths ⁸¹. Atomic line emission is most prevalent after the plasma expansion at lower temperatures as a result of the radiative recombination of the charged particles in the plasma⁷⁰. As a result of the different decay rates of the continuum and the atomic species, the analyst may select the proper detection window when the analyte species emission is the highest.

The LIBS signals are optimized for both the gate delay and the integration time to produce the highest signal-to-noise ratio, corresponding to the best precision and accuracy.

1.6.4 Advantages of LIBS

Simplicity is an important advantage for LIBS, as is being able to analyze all types of materials. Gases, liquids and solids can be analyzed quickly and accurately, with experiments performed at atmospheric pressure. LIBS is a micro-sampling technique and is considered to be virtually non-destructive. The total mass removed per LIBS analysis is in the nanograms range ³¹, allowing for evidence preservation in the forensic laboratory. Little-to-no sample preparation is required as a few laser pulses prior to analysis will remove all contaminants. LIBS is able to provide multi-element detection with no pre-chosen element menu.

An echelle spectrometer covers a very broad spectral range, i.e., 200-900 nm, providing multi-element analysis, with excellent resolution using LIBS. LIBS sampling allows for different analytes of interest to be monitored simultaneously. LIBS provides real-time elemental analyses, with the possibility of *in-situ* analysis and stand-off detection ¹¹⁰. LIBS is often referred to as a semi-quantitative technique, however, recent research has demonstrated LIBS to be capable of quantitative analysis ¹¹¹⁻¹¹³.

1.6.5 Disadvantages of LIBS

Chemical matrix effects may interfere with the calibration and occur when the emission of one element affects the precision of another element. These matrix effects can be corrected if the concentration of the interfering element is known or by choosing another emission line. Special care must be given to non-homogeneous samples. LIBS is a micro technique and when analyzing liquids or gases it is often safe to assume the sample is heterogeneous. Solid analysis cannot assume homogeneity; special attention needs to be given to ensure one is collecting a representative elemental profile of the sample. Representative sampling can be accomplished by sampling at many locations repeated times or to mill the samples and press the resulting powder. LIBS is criticized for not being as sensitive as the other well-established techniques. The sensitivity is largely dependent on the spectrometer used for analysis. However, research has shown LIBS to compete with LA-ICP-MS in the analysis of forensic glass ³.

Another disadvantage often associated with LIBS is the shot-to-shot variability, that is often contributed to the laser-sample interaction ⁷². The lack of matrix matched standards may pose difficult challenges during the solid sampling examination process. Matrix-matched standards are important for quantitative analysis. It is assumed that the laser-material interaction in matrix-matched samples will be similar, therefore removing similar amounts of mass¹¹⁴, thereby producing a similar analytical response and allowing for quantitative analysis. The laser-material interaction will be significantly different between different sample matrices, which require LIBS to use an external calibration.

Many steps are often taken in preparing homogeneous solid samples because they are often unavailable for purchase. For example, pelletizing is the most common way of solid sample preparation. The matrix is ground into a homogeneous powder, which is then pressed into a pellet ideally producing a flat, homogeneous surface. Milling of the sample has been documented to produce homogenous samples¹¹⁵. Shot-to-shot variability

is also overcome by normalization, either to an internal standard or to another emission line within the spectrum and with parameter optimization.

Overall, LIBS is proving to be a competing technique for the elemental analysis of solids, liquids and gases.

1.7 Principles of Laser Ablation Inductively Coupled Mass Spectrometry

Laser ablation inductively coupled mass spectrometry is one of the most successful solid sampling techniques. LA-ICP-MS provides a wide linear dynamic range for detection of major, minor and trace elements.

In 1980, Houk *et al.*¹¹⁶ introduced ICP-MS and the basic set-up has not changed since then. Improvements were achieved in producing lower backgrounds, better sensitivity, user-friendly interface, reduced size and reduced expense^{117,118}. The ICP-MS includes five main parts: 1) Sample introduction, 2) Plasma in torch, 3) Sampler and skimmer cone interfacing between atmospheric pressure and vacuum, 4) Mass spectrometer and 5) Detector¹¹⁹.



Figure 9. Schematic of ICP-MS instrument¹¹⁹

Precision and accuracy is dependent on sample introduction. Sample introduction was initially only for solutions in which a nebulizer produced an aerosol. The aerosol was then transported by a carrier gas into the ICP. The experimental procedure requires all samples to be in solution. In 1985, Gray³⁹ developed laser ablation as a new sample

introduction for ICP-MS. Laser ablation generates particles when the laser-material interaction occurs with the solid sample. A carrier gas then sweeps these particles in the ICP-MS. Today, laser ablation, has eliminated sample preparation time consuming dissolutions, while still providing the sensitivity of ICP-MS. The laser ablation process is reviewed in more detail in section 1.5.

The ionization source is an inductively couple plasma (ICP) torch. It was originally used as an excitation source for optical spectroscopy. The torch consists of three concentric tubes through which argon flows, varying from 5 to 20 L/min¹²⁰. A high radiofrequency is applied to the coil and the argon is ionized by a spark from the Tesla coil. Collisions of the electrons and the resulting ions sustain the plasma. The interaction between the magnetic field and the electrons and ions result in an annular path motion. The plasma is maintained and the torch is protected from melting by different gas flows. The tangential flow of the argon cools the inside walls of the center tubes and centers the plasma. The atoms are ionized by the electron impacts. The atoms will have a resonance time in the plasma for approximately 2 milliseconds at temperatures from 4000-8000 K¹²⁰. The ionization potential of the atoms will determine the degree of ionization. The ionization potential of argon is 15.6 eV. All elements with a significantly lower ionization potential will be 90% or more ionized¹¹⁸.

The first ion extraction occurs in the interface coupling between atmospheric pressure of the torch and vacuum pressure of the mass spectrometer. The connection between the torch and the mass spectrometer is a critical part of the instrument and consists of the sampling and the skimmer cone. The skimmer cone with a diameter of approximately 1 mm is water cooled because of the high temperatures of the plasma.

Following this cone, the pressure is maintained at approximately 1 Torr by a rotary pump. The ions expand rapidly in this region and are cooled. A fraction of these ions then pass through the skimmer cone with a diameter of typically 0.8 mm. Behind the skimmer cone the pressure is maintained at the same pressure of the mass spectrometer using turbomolecular pumps. The ions are separated by a negative potential. The lighter ions are deflected more than the heavy ions as a result of the electrostatic repulsion of the positive charged ions. The remaining ions are then guided in this region by a magnetic ion lens to the entrance of the mass analyzer where they are separated by their mass to charge ratio.

1.7.1 Optimization of LA-ICP-MS

The optimization procedure consisted of measuring and achieving certain target values for certain isotopes. The isotopes and their minimum corresponding values are listed first by isotope, followed in the parenthesis by the minimum target value listed in counts per second. The following isotopes were optimized: ⁷Li (>1500 cps), ⁴⁹Ti (>1000 cps), ⁵⁷Fe (>8000 cps), ⁵⁹Co (>8000 cps), ¹³⁹La (>10000 cps), ¹⁴⁰Ce (>14000 cps), ²³²Th (>3000 cps), ²³⁸U (>3000 cps), ThO/Th fraction needed to be less than 1%, doubly charged interferences needed to be less than 3%, and U/Th was sufficient between 0.7 – 1.3. The instrument is determined to be functioning properly when the above criteria are met.

1.7.2 Advantages of LA-ICP-MS

The introduction of laser ablation to ICP-MS created extra advantages to already the existing advantages of ICP-MS as a solution analytical technique. First, the sample

preparation is greatly reduced as dissolution methods may take several hours with potentially hazardous chemicals. There is less sample handling and reducing contamination. Contamination may be a result of sample containers, solvents and/or the atmosphere. Molecular ion inferences are reduced with no solvents being needed, as in solution analysis. Solid sampling by LA-ICP-MS provides spatially resolved information and depth resolution capability. Total mass ablated is usually nanograms to micrograms¹¹⁴, making the technique virtually non-destructive. Traditional solution methods require milligrams of sample.

LA-ICP-MS is able to offer rapid simultaneous, multi-element detection reaching part per trillion limits of detection with a wide linear dynamic range.

1.7.3 Disadvantages of LA-ICP-MS

LA-ICP-MS is a micro sampling technique and consumes much less mass quantities than that of ICP-MS. Sampling at many random locations has been shown to provide a representative elemental profile of solid samples⁴¹. Solution techniques are known for their tedious, time consuming wet chemistry methods. However, it is possible to produce homogeneous samples with matrix-matched standards.

Similar to LIBS, the lack of matrix matched standards produces difficult challenges during the solid sampling examination and quantitation process. Often numerous steps, such a pelletizing, are used to prepare homogenous solid samples. The elemental sensitivity will be significantly different between different sample matrices, which require LA-ICP-MS to use an external calibration. It is assumed that the laser-

material interaction in matrix-matched samples will be similar, therefore removing similar amounts of mass¹¹⁴ and allowing for quantitative analysis.

Elemental fractionation is defined as the non-stoichiometric effects that occurs during laser ablation and is problematic without matrix matched standards. Fractionation prevents an accurate determination of the elemental concentration. Fractionation has been contributed to but not limited to: ablation, aerosol transport and excitation/vaporization. Mank *et al.* suggested that fractionation is a result of crater depth to crater diameter ratio which will affect particle ejection and particle melting¹²¹ and Horn *et al.* contributed it also to crater diameter¹²². Enhanced sensitivity was reported by Eggins *et al.* by using a helium/argon mixture as the carrier gas¹²³. Laser ablation is responsible for the particle size and Houk *et al.* demonstrated that not all particles are vaporized within the ICP^{124,125}. Russo *et al.* demonstrated that greater laser irradiances and shorter pulse widths decreases fractionation by producing smaller size particles which are transported more readily and efficiently ionized and atomized by the inductively coupled plasma¹¹⁴.

1.8 Microdrop Printing

Microdrop printing is a contactless method for depositing precise sub-nanoliter volumes of solutions and is able to deliver drops ranging in diameter from a few microns to tenths of a millimeter, depending on nozzle orifice. Verkouteren *et al.* reported the standard uncertainties for microdrop dispensing to be approximately 1%. Microdrop printing has the ability to deliver a wide range of solvent¹²⁶ and aqueous¹²⁷ based solutions, making the microdrop dispensing technique common in many analytical applications.

Microdrop printing from a nozzle was documented as early as 1833 by Savart¹²⁸ and in 1878 Rayleigh¹²⁹ where they described the continuous mode inkjet printing technique. Here a pressure wave inside the capillary pushes the fluid from the nozzle orifice to produce uniform sized microdrops. As the drops fall into an electrostatic field, they acquire a charge and are focused to a location on the substrate. The variation in the charge applied will influence the microdrop trajectories.

Development of continuous mode inkjet printing continued to flourish. Dr. Sweets of Stanford University demonstrated a similar concept as above, the difference being that the fluid stream can be fragmented into microdrops of uniform size and spacing with an applied pressure wave¹³⁰. The microdrops that acquired a charge in the electric field were focused into a reservoir for recirculation and the uncharged drops would fall onto to substrate¹³⁰. IBM licensed this technology in the 1970's to develop the technology for their computer printers.

A significant development by Hansell in 1950 patented the production of drops by an induced pressure wave¹³¹. A voltage pulse is applied to a piezoelectric material

resulting in a volumetric change causing pressure in the fluid to produce a drop from the nozzle orifice. This documented the drop-on-demand mode, as the drop was only produced by an applied voltage. This technology flourished in the late 1970's as it was simpler than the continuous mode inkjet printing as a result of no fluid recirculation. The invention of drop-on-demand was also used for commercial printers and the ink microdrops were delivered by pressure wave of the piezoelectric ceramic.

Today drop-on-demand inkjet systems are more commonly used than continuous mode systems. However, both continuous and drop-on-demand modes are widespread. Continuous mode inkjet printing is mostly used industrially for product labeling of foods and medicines and drop-on-demand mode inkjet printing are most commonly used in the typical office printer.

Microdrop printing has many characteristics that make it appealing for many different analytical applications. It is a non-contact method that is not dependent on how wet the printed substrate becomes. The source of the fluid cannot be contaminated by the matrix during the inkjet dispensing. With the documented error rate of approximately 1% for drop production¹²⁶, very precise volumes and mass quantities can be deposited.

Inkjet printing is currently being used for many applications. Sirringhaus *et al.* used inkjet printing on thin film transistors to produce electrodes on a glass substrate. They created channel lengths from sub micrometer to tens of nanometers¹³². Inkjet printing is also used for combinatorial studies because it is a direct writing process as it does not require the use of writing masks. Tekin *et al.* examined the emission properties using inkjet printing of different polymers with different side chains and film thicknesses¹³³. Inkjet printing has been used to print organic, inorganic and hybrid

inorganic/organic solar cells^{134,135}. The deposition of nanoparticles using inkjet printing is becoming popular. Voit *et al.* deposited magnetic nanoparticles of iron oxide¹³⁶. Crowley *et al.* printed nanoparticles to produce an ammonia sensor¹³⁷. Microdrop printing has been used extensively for a long period of time in biological applications, as a result of vesicles being nanometer size. Vesicles are used in drug screening for living cells and play an important role in endocytosis and exocytosis processes^{138,139}.

A demand in analytical chemistry exists to develop techniques for the analysis of ultra-small volumes. However, there is less research conducted in analytical chemistry using microdrops for chemical analysis. Microdrop printing allows for sub-nanoliter volume delivery. Currently, most research in this area has been conducted by Hahn and Niemax. These authors have demonstrated that microdrops deposited on Si-wafers can be used for analyte standards¹⁴⁰. They conducted further studies with microdrops using analytical plasmas of ICP and LIBS. The microdrops were deposited into the plasma and linear calibration curves were constructed for each of both ICP and LIBS, demonstrating the potential for single drop analysis¹⁴¹. Pioneering research presented in Chapter 5, demonstrates that LIBS is capable of microdrop quantification analysis using picoliter volumes¹¹³.

1.8.1 Piezoelectric Microdrop Printing

The piezoelectric inkjet can be classified into four different categories: squeeze, bend, push and shear¹⁴². The bend mode forms a transducer by bonding the piezoceramic plates to the diaphragm used to form the microdrops. Piezoceramic rods expand to push against the fluid and eject microdrops in the push mode. In the shear mode the

microdrops are formed and ejected by the deformation of the piezoplates pushing against the fluid. The squeeze mode, the most successful design, the glass nozzle is surrounded by a thin tube of piezoceramic. In the squeeze mode with the tubular piezo actuator surrounding the glass capillary, a voltage is applied to abruptly compress the enclosed fluid and produce a pressure wave that propagates through the glass capillary into the fluid. The pressure wave travels though the fluid and accelerates in the region of the nozzle, resulting in the ejection of a microdrop at the nozzle orifice that will fall freely in air.

Monodisperse microdrops are formed under optimized conditions. The following parameters are optimized though trial and error: drive pulse amplitude, drive pulse shape, internal pressure level, drop ejection rate and the fluid fill level. The drive amplitude will affect the size of the drop and the drop ejection velocity. The microdrop ejection speed will vary from approximately 1 to 10 m/s¹⁴³. Optimization of the pressure pulse rise and fall times will produce satellite free microdrops. Satellites or randomly sized drops will be formed if the amplitude of the pulse is too great.

The drop ejection process is determined by the drive waveform used for the piezoelectric actuator, see Figure 10. The optimum conditions are defined by achieving the highest drop velocity for the amplitude pulse. The first half of the waveform is controls the fluid expansion, the delay for pressure wave propagation and fluid compression. This creates the negative pressure initially and creates a pressure rise. The second half of the waveform is to cancel residual oscillations that remain after drop ejection¹⁴⁴.



Figure 10. Piezoelectric waveform for inkjet printing¹⁴⁴

Through trial and error the parameters were optimized. It was noted that shorter pulse widths will produce smaller drops, higher amplitudes are needed to eject microdrops with shorter pulse widths, the microdrops are primarily determined by the diameter of the nozzle orifice, changing the pulse width can alter the microdrop direction and a wet nozzle orifice may stop the production of drops.

1.8.2 Terminal Velocity of Microdrops

The atmosphere is made up of gas molecules, as an object moves through the atmosphere; these molecules are disturbed and will move around the object. It is easier to explain the interaction of two solid objects. When two solid objects interact, forces are transmitted at the point of contact. However, when a solid is immersed in a fluid media, such as air, the fluid is able to maintain contact at all points by flowing around the object.

If the fluid is in motion, the direction of this motion can be defined. The lift is defined as the net force perpendicular to the flow direction and the drag is the net force with the direction of flow. These same forces are generated between the atmospheric gases and an object, such as a microdrop. The magnitudes of these forces are dependent of the object shape and speed and the mass and viscosity of the gas. The Reynolds number, R_e, is a measure of the viscosity and defined as

$$R_e = \frac{vd}{v} \propto \frac{dynamic \, pressure \, force}{viscous \, force} \tag{9}$$

where v is the drop velocity relative to air, d is the drop diameter, v is the kinematic viscosity (air is $0.151 \text{ cm}^2/\text{sec}$ at standard temperature and pressure) which equals η/ρ where η is the viscosity of air (1.82 x 10⁻⁶ gram/cm-sec at standard temperature and pressure) and ρ is the density of air (0.001206 gram/cm³)¹⁴³.

In fluid mechanics the Reynolds number, represents the ratio of inertial forces to viscous forces in a fluid. The Reynolds number is dimensionless and high values indicate viscous forces are small, low values indicate that viscous forces dominate.

Many applications involve the drag coefficient of a sphere for spherical or nearspherical object, i.e., particles and droplets. The flow around the sphere is laminar and for Reynolds numbers of less than 0.5, the force required though a viscous fluid at a specific velocity is defined by Stokes' Law¹⁴⁵. George Gabriel Stokes discovered that when a spherical object falls through a fluid medium, the first layer of the fluid adheres to the spherical object and will travel along with at the identical velocity. It is a linear process as the next layer will have less velocity and so on, while the layer at furthest distance will remain at rest. The results are a dragging force upward, opposing the downward motion of the spherical object, called the viscous force^{145,146}. The velocity of the falling object will increase as does the viscous force till the viscous force equals the body weight. This is known as terminal velocity. Stokes defined the viscous force by

$$F_d = 6\pi\eta r v \tag{10}$$

where F_d is the drag force (resistance) of the fluid on the spherical object, η is the viscosity of the fluid, *r* is the drop radius and *v* is the drop velocity. To better understand this concept a free body diagram of a sphere is constructed. The sphere demonstrates the different forces, internal and external, that are encountered in the fluid (e.g., air), see Figure 11¹⁴⁷.



Figure 11. Stokes sphere forces¹⁴⁷

The sphere seen in Figure 11 has three acting forces, two being upward forces and one being from the downward force. The two upward forces are a result of: 1) the displacement of the weight of the fluid, also referred to as the buoyancy effect¹⁴⁶, F_b , acting vertically upwards and 2) the viscous/drag force resisting the gravity acceleration, F_d . The only downward force is the weight of the spherical object falling. It is defined by the gravitation attraction (F=mg). The terminal velocity of a microdrop in air is calculated by setting both the upward drag forces equal to the gravitational force on the drop¹⁴³. The sum of all forces equals

$$F_d + F_b = mg \tag{11}$$

where *m* is the mass of the spherical object and *g* is the gravitation force (9.807 m/s²). Knowing that the volume of a sphere is given by

$$v_{sphere} = \frac{4}{3}\pi r^3 \tag{12}$$

and combining this with the ρ being the density of the material and σ being the viscous density of the medium, the following two equations are developed

$$mg_{=\frac{4}{3}}\pi r^{3}\rho g \tag{13}$$

$$F_b = \frac{4}{3}\pi r^3 \sigma g \tag{14}$$

Therefore the combination of these equations produces

$$F_{b,mg} = \frac{4}{3}\pi r^3(\rho - \sigma)g \tag{15}$$

After rearranging the above terms, the terminal velocity, v, is solved for

$$v = 2r^2(\rho - \sigma)g/9\eta \tag{16}$$

The viscosity of the medium, in the case of microdrops is air. Stokes resistance is the energy that is required to orderly deform the air so that the microdrop can pass through. Stokes drag force for microdrops is first order independent and is linear with velocity¹⁴³. The Stokes drag force for microdrops is different from dynamic pressure sources associated with large objects, such as an aircraft. The drag at high Reynolds number (R_e >10³), is dependent on the square of the velocity. The terminal velocity of microdrops will be discussed further in section 5.5.2.

2 Wavelength Dependence of the Forensic Analysis of Glass by Laser Induced Breakdown Spectroscopy

Most LIBS studies and commercial instrumentation utilize the IR 1064 nm laser, as a result of its higher power and lower cost of acquisition. However when searching through literature, it is the lower wavelengths that provide better analytical figures of merit for LA-ICP-MS studies¹⁴⁸. The preferred laser wavelength for most LA-ICP-MS instrumentation is the fourth or fifth harmonic as it provides better laser-material interaction. It is for reason, I have investigated and compared the UV (266 nm) laser and the more widely used IR (1064 nm) wavelength for LIBS analysis of float glass³¹.

2.1 Experimental Instrumentation

The LIBS instrumentation presented in this work consisted of different single-pulse and double-pulse wavelength configurations. The LIBS system built in our laboratory consists of a Q-switched Nd:YAG NewWave Research Tempest laser (New Wave Research, Fremont, CA) operating at the fourth harmonic (266 nm) and a second Nd:YAG Big Sky laser (Big Sky, MT) operating at the fundamental wavelength of 1064 nm, both having pulse widths of 3-5 ns full width half max. Flashlamps and Q-switches were both externally controlled by a Berkeley Nucleonics (San Rafael, CA) delay generator model 656. Beam expanders were used to enlarge the beams from ~4 mm to nearly 12 mm using a Galilean telescope. The beams were then focused at a normal incidence to the sample through a plano-convex lens with a focal length of 150 mm, see Figure 5, with a 90^0 viewing angle to the laser.

To ensure representative sampling and to account for any heterogeneity, each glass standard was analyzed 5 times at different locations. Both single-pulse and double-pulse spectra were collected as a result of 100 laser shots with the accumulation of the last 50 shots used to generate the spectra for analysis conducted at atmospheric pressure in air.

In order to gain the best reproducible optical emission spectra possible, both the 266 nm and the 1064 nm experiments were optimized for laser power, lens-to-sample surface-distance (LTSD), gate delay, and integration time.



Figure 12. Lens-to-sample distance optimization for LIBS glass analysis for background subtracted intensity or Lorentzian fit peak areas for a) Sr I 460.7 nm or b) Al I 394.4 nm
The laser energies for the single-pulse UV ablation was held at constant values throughout the experiments at 29 mJ for the 266 nm laser. The laser was focused 1.30 mm into the sample surface during the 266 nm experiment. Figure 12 demonstrates that the best precision was achieved for the 266 nm laser at a LTSD of 1.3 mm for both background subtracted intensity and Lorentzian fit peak areas.

The laser energy for the single-pulse IR 1064 ablation was held at constant value throughout the experiment of 47 mJ. Figure 13 demonstrates the precision with the variance of laser energy. In forensic science, evidence preservation is important, and with an energy above 47 mJ the colorless glass fragment would be destroyed. Figure 17 shows the damage that is caused by IR 1064 nm laser interaction with colorless glass and the irregular crater morphology that is produced.

The IR 1064 nm laser was focused 0.50 mm into the surface for the 1064 nm experiment. The optimized energy and LTSD allowed for the least destruction of the sample while still providing analytical signal.



Figure 13. Precision variation with laser energy on glass using 1064 nm laser

A Scanning Electron Microscope (SEM) Philips XL 30 with EDX detector (Philips, The Netherlands and EDAX, USA, respectively) was used for the imaging of the craters created by UV and IR ablation. The amount of mass ablated was calculated using the density and volume. Using a glass density of 2.5 g/cm³, the volume was converted to nanograms removed.

The laser beams are focused perpendicular and parallel to the sample to create either single-pulse ablation or double-pulse prespark or plasma reheating schemes. The geometric configurations for double-pulse LIBS were optimized as follows; the orthogonal configuration included one beam perpendicular to the surface while the other pulse was parallel to the surface. During prespark experiment, the IR beam was focused 0.75 mm above the sample surface at 160 mJ creating a spark in air followed 7 μ s later by the perpendicular UV ablation pulse at 29 mJ. Figure 14 below demonstrates that at 7 μ s the greatest increase in intensity was observed.



Figure 14. Optimized double-pulse LIBS prespark interpulse delay

In the plasma reheat configuration, the UV ablation beam was pulsed at an energy of 27 mJ, followed 400 ns later by a 35 mJ IR beam, focused 0.75 mm above the sample to reheat the plasma. Figure 15 shows the analytical signal during DP LIBS reheat to be at maximum signal with good precision at a delay of 400 ns.



Figure 15. Optimized double-pulse LIBS reheat interpulse delay

Optical emissions from the plasma were acquired from the side (90°) by a pair of plano-convex lenses (f = 75 mm) onto a fiber with a diameter of 50 µm that was coupled to the entrance slit of an Andor Mechelle 5000 spectrometer equipped with an Andor iStar intensified CCD camera using a 1024 X 1024 chip. The optimized gate delays for both the 266 nm and 1064 nm experiments were 1.2 µs, while the optimized integration time was 3.5 µs and 11.0 µs for the 266 nm and the 1064 nm wavelengths, respectively. The broadband detector captured the spectral range between 200-950 nm with a resolution of ~ 5000. As a result of the broadband spectral analysis, the repetition rate for the spectrometer was ~ 0.67 Hz.

Analytical glass standards from National Institute of Standard and Technology (NIST) 614, 610, 612, 1831 and Bundeskriminalamt (BKA) glass reference standards

FGS 01 and FGS 02 were used for development of the analytical protocols and to determine the precision, accuracy and repeatability of the LIBS analysis.

2.2 Effects of Laser Wavelength

The laser wavelength, pulse energy and irradiance are important properties and are responsible for producing a laser induced analytical plasma. The effect of laser wavelength influences the laser-material interaction as a result certain wavelengths will couple more efficiently with specific material and the plasma-material interaction. It has been documented that shorter wavelengths will produce increased photon energies which will aid in the ionization process⁷⁰. For example, the 193 nm wavelength laser has a photon energy of 6.4 eV compared to only 1.15 eV for the 1064 nm laser. With sufficient photon energy, the ablation process will occur by photon ionization and non-thermal mechanisms⁷⁰.

The plasma is produced by sample surface vaporization and absorption of the laser energy in the ablated material. The amount of ablated mass as a result of material-nanosecond laser interactions has been shown to vary significantly with the use of high power nanosecond laser irradiation¹⁴⁹. The varation is a result of the high flux density and the ablated material being heat by the tailing end of the laser light.

Commercial laser ablation systems are now equipped with shorter wavelengths, i.e. 193nm, 213 nm or 266 nm because it has been shown that UV wavelengths provide more laser energy per unit volume for ablation, resulting in increased mass removal¹⁵⁰ compared to IR ablation, better crater morphology³¹ and improved reproducibility of

signal³¹, demonstrating that the shorter wavelengths provide a more controlled ablation rate ^{30,150,150}.

Several researchers have reported results from the use of different wavelengths ranging from the plasma characteristics such as temperature and density³⁰, plasma formation¹⁵¹, fractionation¹⁵⁰, laser-sample coupling^{150,152}, and quantification of analytical results^{30,153}. The coupling of the laser energy to the sample is clearly affected by the irradiation wavelength. Previous studies have shown that the UV wavelength can improve the coupling efficiency when compared to the longer wavelengths, i.e., 532 nm and 1064 nm^{30,150}.

2.2.1 Crater Morphology

Crater morphology influences the analytical results. LIBS on solid surfaces is dependent of the material ablated into the plasma plume⁷². LTSD is a critical parameter for LIBS measurements. A change in the depth of focus can affect the LIBS signal and reproducibility. Experimental trials demonstrated that by defocusing the beam, forcing the laser to focus into the surface, the reproducibility of the LIBS emission signals improved. The experimental trials determined that focusing the 1064 irradiance laser into the surface prevented shattering the glass, see Figure 16. The optimal LTSD determined for both the 1064 nm and 266 nm wavelengths were 0.50 mm and 1.30 mm focused into the sample, respectively.

The amount of mass ablated per laser pulse per unit area is defined as the ablation rate. LIBS typically removes mass from the sample in the ng-µg range, classifying it as a surface sampling technique. However, multiple pulses at the same location can be used

to progressively ablate the surface, thereby removing more material and permitting depth profiling or bulk analysis of the sample. Researchers have reported that the 266 nm ablation removes more mass than the 532 nm or 1064 nm^{30,150,152,153} ablation experiments, which is a result of the better energy coupling efficiency provided by the UV, combined with less plasma shielding.



Figure 16. The damage caused to glass using IR 1064 nm laser

The crater diameter has been proven independent of the sample matrix, while the crater depth is dependent on sample matrix¹⁵⁴. Previous conducted research has theorized that more mass ablated with minimal sample heating can provide a more stoichiometric sampling¹⁵⁰. Analytical research has been conducted demonstrating that the IR plasma is hotter¹⁵⁵, which will increase the plasma shielding and reduce the amount of the IR energy that can be transferred to the sample surface¹⁵⁶.

The crater morphology can be appreciated at a high 1000 times magnification as shown in Figure 17, demonstrating the differences for 100 shot ablations from the 266 nm ablations (Fig. 17a) compared to the 1064 nm ablations (Fig. 17b). Crater morphology produced at these lens-to-sample-distance (LTSDs) resulted in a diameter of 75 μ m and depth of 70 μ m for the 266 nm laser and a diameter of 37 μ m and depth of 26 μ m for the 1064 nm laser. The total mass removed by the 266 nm ablation was found to be ~790 ng, approximately ten times higher than the 81 ng of the 1064 nm laser. The data acquired supports the theory that UV wavelengths, as a result their higher photonic energy, provide photoionization and/or multiphoton ionization.



Figure 17. a) Crater formed using a 266 nm laser on NIST glass standard 1831 b) Crater formed using a 1064 nm laser on NIST glass standard 1831

Research studies determined that the differences of the mass removed between the single and double-pulse LIBS ablations was negligible; this is in agreement with previous research conducted by Santagata *et al*¹⁵⁷. However, this contradicts research reported by Scaffidi *et al.*, where they reported an eight to ten fold increase in mass ablated using the orthogonal double-pulse configuration¹⁰¹. Investigation of the crater morphology also reveals a more uniform crater produce by the 266 nm laser, which may translate to better precision in LIBS measurements.

2.3 Quantitative Analysis

Quantitative analysis by LIBS is not standardized and many quantification methods have been proposed for chemical analyses. One of the key reasons for the proposal of different methods is because of the lack of standard reference materials. However, the availability of glass standard reference materials permits calibration curves for the quantitative chemical analyses and calibration curves have been proven effective for many years.

Construction of the calibration curves were produced by the line intensities (max counts of intensity minus the background) in correlation to the corresponding elemental concentration of the glass standard. Each point on the calibration curves represents an average of five replicates, with the second 50 of 100 shots being averaged. The vertical error bars are represented as \pm 1 standard deviation calculated from the 5 replicates. The calibration curves of the different atomic lines of the same element were very reproducible (see the error bars in figures 19a-19f) and were utilized for the quantification of trace elements in glass. All chosen spectral lines have minimal spectral interferences. LIBS produced sharp emission lines allowing for qualitative and quantitative analysis. Spectral peaks for emission lines Ba II 493 nm (32 ppm), K I 766 nm (2738 ppm), and Sr II 421 nm (89 ppm) can be seen in Figure 18 below for the different LIBS configurations of SP UV LIBS, SP IR LIBS and DP UV ablation IR reheat.



Figure 18. Spectral emission lines for a) Ba II 493.4 nm (32 ppm), b) K I 766.5 nm (2738 ppm) and c)

Sr II 421 nm (89 ppm)

The five glass standard reference materials and their corresponding concentrations are listed in Table 1. NIST glass standard 1831 is a float glass formulation and was analyzed twice for this study, with the second set of measurements treated as an "unknown" sample for comparison purposes.

Element Concentrations for Glass Reference Materials (µg/g)						
CRM	Sr	Ba	Al	К	Mg	Ti
1831	89	32	6381	2738	2116	114
610	497	424	10006	486	465	434
612	76	38	11165	66	77	48
FGS 1	57	40	1500	920	23900	69
FGS 2	253	199	7400	4600	23400	326

Table 1. Certified Concentration of Glass Standards (µg/g)

Limits of detection (LOD) and limits of quantification (LOQ) were calculated according to LOD= $3s_B$ and LOQ= $10s_B$, where s_B is the standard deviation of the background, which is taken as close to the emission line as possible without encountering spectral interferences. Trace elements K I 766.49 nm, Ba II 493.41 nm, Sr II 407.77 nm and Ti II 336.12 nm, were chosen as a result of previous work by our group, demonstrating the high discriminating power of these elements in the glass matrix³.

2.3.1 Single-Pulse Quantitative Analysis

Single-pulse LIBS spectra were acquired as previously described using both by 266 nm and 1064 nm lasers. The experimental conditions that provided the highest precision and

accuracy were determined and used throughout the study.

The energy of the 266 nm laser was held constant at 29 mJ, while the 1064 nm laser was held at 47 mJ. It was found that at these energies the reproducibility of the experiments increased and limiting the IR wavelength to 47 mJ prevented cracking and damaging of the glass during ablation. A detector delay of 1.20 µs was used, which allowed for the decay of background continuum and production of sharp emission lines. Figure 19 illustrates calibration curves produced by single-pulse 266 and 1064 nm. Each measurement corresponds to the intensity of the emission line of interest obtained with an accumulation on the detector of the second 50 accumulation of 100 laser shots. Single-pulse UV and IR configurations demonstrate good correlation with most R² values being greater than 0.990. It has been demonstrated in previous research that IR irradiances show greater enhancement with ionic emission lines⁹⁸, this is witnessed when comparing K I 766.5 nm and Sr II 407.7 nm.









Figure 19. a) Single-pulse 1064 nm calibration curves for K I 766.5 nm; b) Single-Pulse 266 nm calibration curve for K I 766.5 nm; c) Single-pulse 1064 nm calibration curves for Sr II 407.7; d) Single-Pulse 266 nm calibration curve for Sr II 407.7; e) Single-pulse 1064 nm calibration curves for

Ba II 493.4; f) Single-Pulse 266 nm calibration curve for Ba II 493.4

As mentioned earlier in this paper, NIST 1831 standard was chosen and analyzed twice, the second time being treated as an "unknown" sample. As both methods show good correlation, the UV irradiance demonstrated better precision for the K and Sr lines. The IR irradiance proved to have lower limits of detection, however, in trace elemental analysis of glass, the LOD obtained by UV LIBS ablation would provide sufficient sensitivity for the chemical characterization of glass, see Table 2.

Method	Sample	Peak (nm)	Precision (%)	Bias (%)	LOD (ppm)	LOQ (ppm)
SP UV	1831	K I 766.5	8.23	12.15	5.93	19.77
SP UV	1831	Sr II 407.7	5.80	16.82	4.10	13.68
SP UV	1831	Ba II 493.4	10.83	9.48	2.25	7.51

Table 2. Figures of Merit for the Single-Pulse UV 266 nm (SP UV)

2.3.2 Double-Pulse Quantitative Analysis

Double-pulse LIBS has gained merit over the recent years. Improvements in the figures of merit by double-laser pulse configurations have contributed to better sensitivity and signal gain for LIBS analyses^{98,99}. Several double-pulse geometric configuration approaches have been used consisting of either one laser¹⁵⁸, or two different lasers¹⁵⁹ to encompass a double-pulse LIBS setup.

Orthogonal pre-spark and plasma reheat were the two configurations used during this work. Optimal separation time between the two laser pulses was determined by plotting the LIBS emission intensity versus the delay time. The main objective of this study was not given to the highest intensity enhancement, but rather to increased precision and accuracy. Demonstrated in this study, an intensity decrease is seen from single-pulse to double-pulse orientation. The decrease in signal was also reported by Gautier *et al.*⁹⁸, when they observed lower line emissions using UV ablation, from elements with lower excitation energies of approximately 4 eV, in the double-pulse reheating approach when compared to single-pulse. The elements of interest investigated here all have lower excitation energies of 1.6, 3.0, and 2.5 eV for K I 766.5 nm, Sr II 407.7 nm, and Ba II 493.4 nm, respectively, which could account for the witnessed decrease in intensity.

Double-pulse plasma reheat has been attributed to higher plasma temperatures and electron densities because of the larger plasma size after the second plasma reheat beam, which would allow for longer integration times. As can be seen by Figure 20, all correlation coefficients are greater than 0.990, demonstrating very good linearity. The precision demonstrated by the plasma reheat scheme is moderately lower than that by single-pulse UV, which has also been reported by Scaffidi *et al.*¹⁶⁰, and comparable to that of single-pulse IR configuration. As emission enhancement is not seen, however, most LODs have decreased. The LOD for K I 766.5 nm and Sr II 407.7 nm have decreased from the single-pulse value of 5.93 and 4.10 ppm to 4.30 and 3.17 ppm, respectively, showing an increase in the double-pulse plasma reheat sensitivity, see Table 3.





Figure 20. Calibration curves for double-pulse plasma reheat with 266 nm ablation for a) K I 766.5 nm and b) Ba II 493.4 nm

Prespark LIBS is theorized to cause ambient gas breakdown before the ablation pulse is produced, creating different effects that could lead to an increased emission by the analyte. It was hypothesized that the reduction in ambient gas causes the plasma to expand faster, thereby reaching a larger size, while producing less plasma shielding for the ablation pulse^{106,161}. Higher sensitivity was also evident in the double pulse prespark configuration, than when compared to all other experimental data, because of the resolution of emission line Ti II 336.12 nm. Emission line Ti II 336.12 nm was pronounced and a linear correlation achieved, see Figure 21, while in the other configurations the Ti II line was not resolved well enough for calibration. As seen in the plasma reheat configuration coefficients most greater than 0.990. However, the prespark shows less precision than that demonstrated by either the UV/IR single-pulse or the plasma reheat, see Table 3.



Figure 21. Calibration curves for double-pulse IR pre-spark with 266 nm ablation for a) K I 766.5 nm and b) Ti II 336.1 nm

The reproducibility of each point in the calibration curve was 10-15%. The accuracy of the analysis was evaluated to be ~10%. The determined limits of detection for metal ions in this work were certainly comparable, if not lower with those reported in other publications. Kurniawan *et al.* performed quantitative analysis on glass samples and reported the LODs for Ba, K, and Ti were 190 ppm, 190 ppm, and 410 ppm, respectively¹⁶². Ismail *et al.* reported the LOD of Ti to be 100 ppm for single-pulse and 10 ppm for double-pulse, Yamamoto *et al.* detected Ba and Sr in toxic soil and produced a LOD of 265 ppm and 42 ppm, respectively, and Cremers *et al.* detected Ba in soil to

have an LOD of 26 ppm¹⁶³⁻¹⁶⁵. This exhibits the evolution LIBS is making as a choice analytical technique in the forensic science community.

 Table 3. LIBS Figures of Merit for Single-Pulse, Double-Pulse Reheat, Double-Pulse Prespark and
 Single-Pulse 1064 nm Laser

Method	Sample	Peak (nm)	Precision (%)	Bias (%)	LOD (ppm)	LOQ (ppm)
SP UV	1831	K I 766.5	8.23	12.15	5.93	19.77
SP UV	1831	Sr II 407.7	5.80	16.82	4.10	13.68
SP UV	1831	Ba II 493.4	10.83	9.48	2.25	7.51
DP Reheat	1831	K I 766.5	3.61	14.82	4.30	14.34
DP Reheat	1831	Sr II 407.7	8.43	5.89	3.17	10.56
DP Reheat	1831	Ba II 493.4	12.38	19.95	1.72	5.73
DP PS	1831	K I 766.5	10.45	19.06	3.77	12.58
DP PS	1831	Sr II 407.7	30.38	47.74	3.02	10.07
DP PS	1831	Ti II 336.1	31.67	42.13	11.03	36.77
SP IR	1831	K I 766.5	9.13	16.50	4.07	13.56
SP IR	1831	Sr II 407.7	8.26	8.98	3.28	10.92
SP IR	1831	Ba II 493.4	4.51	39.68	1.98	6.59

2.4 Conclusions

The LIBS technique has increasingly gained attention as a competitive analytical tool for surface analysis, depth profiling, and bulk analysis of solids. Laser wavelength and laser energy play an influential role in analytical performance for LIBS due to the laser-material interaction and the initiation of the plasma.

In the current work, correlation coefficients of >0.990 were achieved for calibration curves for the trace elements analyzed in the range between 32 and 4600 ppm. Precision and accuracy for the quantitative analysis of standards ranged from as good as 4.5% RSD for the precision of glass at 32 ppm for the measurement of Ba and an accuracy of 9.0% bias but more typically resulting in 9–10% RSD for the precision and 10% bias for most elements of interest in these glasses for both the UV and IR experiments and the single- and double-pulse experiments.

The IR ablations resulted in typically less emission intensities, an indication that less mass was ablated when IR was used. Less mass being ablated with the IR nm laser was corroborated with mass removal calculations as the ablation rate between the IR and UV produced significant differences. The plasma shielding was demonstrated to be less with UV irradiance and the laser-sample energy coupling was more efficient with the UV, resulting in better precision and accuracy in most but not all experimental configurations. The UV irradiation produced a more uniform crater, translating to better precision from better signal reproducibility. The craters formed resulting from IR irradiance, even when higher power than UV was used, resulted in less mass ablated and severe cracking and damage to the sample surface, in comparison to the UV.

The LODs for the elements of interest in forensic glass analysis were adequate for the proper characterization and comparison of glass using any of the UV and IR configurations performed in this study. The same emission lines where used in the comparisons for all configurations and, under these comparison conditions, it was concluded that the use of 266 nm irradiation was recommended for the forensic analysis and comparison of glass with single-pulse experiments providing very good analytical data and minimal sample damage.

3 Discrimination and Association of Float Glass by Laser Induced Breakdown Spectroscopy from Single Manufacturing Plants

Laser induced breakdown spectroscopy is an emerging analytical technique for the forensic association and discrimination of glass. The emission intensities are utilized in LIBS in the ultraviolet, visible and near infrared spectrum. The LOD for LIBS will vary with each element but it has been documented to achieve LODs as low as ~2 ppm for the Ba II 493.4 nm and Sr II 407.7 nm, and 4 ppm for the K I 766.5 nm emission line ³¹. These LODs are sufficient for the forensic analysis of glass. The LIBS research conducted to date has been successful in the forensic analysis of glass ^{3,13,28,42}. Naes *et al.* reported that LIBS produces the same 99% discrimination, with no false exclusions, as μ XRF and LA-ICP-MS with a different element menu of automobile float glass ³. Bridge *et al.* achieved an 83% and 74% discrimination of automobile float glass with LIBS, however when combined with refractive index measurements, the discrimination increased to 99% discrimination for both sample sets ^{13,42}. The precision obtained from both authors were in agreement, Naes *et al.* states the precision less than 10% RSD and Bridge *et al.* states an average precision of 7% RSD.

The advantages offered by LIBS include a sensitive and fast approach to elemental analysis and LIBS permits small sample size with good precision, similar to LA-ICP-MS. The instrumentation of LIBS is fairly inexpensive when compared to the more established techniques of LA-ICP-MS, LA-ICP-OES and μ XRF, it is less complex, generates data virtually instantaneously, has the capability to be portable, while providing

high sample throughput. Common disadvantages often described are shot-to-shot irreproducibility, high continuum background, line broadening and self-absorption.

Float glass lines are designed to operate 365 days a year. Typically, 300-600 tons of glass per day are produced in float glass furnaces of which mostly is for architectural and automotive glass products ²⁰. To date, however, no studies have been reported presenting LIBS for the association and discrimination of float glass from a single plant over periods of time. This chapter focuses on the capability for LIBS to discriminate and associate float glass produced at the same plant at approximately the same time period, i.e., from days apart to years apart.

3.1 Float Glass Sample Descriptions

All samples were examined on the non-float surfaces of the respective glass. National Institute of Standards and Technology (NIST) certified reference material (CRM) float glass 1831was included into the experimental procedure to evaluate bias, precision and accuracy, due to the similar matrix. Duplicate samples were analyzed repeatedly throughout experimental procedure as a positive control for method validation to assess type I error. Float glass samples ranging from days apart to years apart were collected from manufacturing plants in the United States to determine the capability of LIBS for forensic glass analysis from single manufacturing plants.

3.1.1 Sample Set 1: Cardinal Glass Industries

Sample set one is composed of 49 colorless float glass samples manufactured in Cardinal Glass Industries (Portage, WI, USA) from May 1997 to September 2001. All the

fragments were clear float glasses that ranged in refractive index from 1.51817 -

1.51905. Table 2 summarizes sample set one.

Source	Sample Description	Color	RI
Cardinal	5/16/1997	Clear	1.51848
Cardinal	7/15/1997	Clear	1.51817
Cardinal	7/18/1997	Clear	1.51841
Cardinal	8/17/1997	Clear	1.51840
Cardinal	9/16/1997	Clear	1.51837
Cardinal	10/15/1997	Clear	1.51838
Cardinal	11/15/1997	Clear	1.51840
Cardinal	12/15/1997	Clear	1.51841
Cardinal	1/14/1998	Clear	1.51835
Cardinal	2/15/1998	Clear	1.51817
Cardinal	4/15/1998	Clear	1.51878
Cardinal	5/17/1998	Clear	1.51897
Cardinal	6/14/1998	Clear	1.51880
Cardinal	7/17/1998	Clear	1.51870
Cardinal	8/12/1998	Clear	1.51869
Cardinal	9/20/1998	Clear	1.51881
Cardinal	11/14/1998	Clear	1.51902
Cardinal	1/15/1999	Clear	1.51882
Cardinal	3/15/1999	Clear	1.51901
Cardinal	4/14/1999	Clear	1.51894
Cardinal	5/20/1999	Clear	1.51895
Cardinal	6/11/1999	Clear	1.51905
Cardinal	7/10/1999	Clear	1.51898
Cardinal	8/19/1999	Clear	1.51895
Cardinal	9/14/1999	Clear	1.51884
Cardinal	10/18/1999	Clear	1.51902
Cardinal	11/24/1999	Clear	1.51889
Cardinal	12/13/1999	Clear	1.51878
Cardinal	1/1/2000	Clear	1.51887
Cardinal	1/18/2000	Clear	1.51879
Cardinal	2/1/2000	Clear	1.51865
Cardinal	2/24/2000	Clear	1.51892
Cardinal	3/1/2000	Clear	1.51890
Cardinal	3/27/2000	Clear	1.51877
Cardinal	4/1/2000	Clear	1.51878
Cardinal	4/16/2000	Clear	1.51882

Table 4. Sample Set 1, Cardinal Glass Industries

Source	Sample Description	Color	RI
Cardinal	5/1/2000	Clear	1.51876
Cardinal	6/1/2000	Clear	1.51875
Cardinal	10/1/2000	Clear	1.51870
Cardinal	11/1/2000	Clear	1.51862
Cardinal	12/1/2000	Clear	1.51874
Cardinal	1/1/2001	Clear	1.51880
Cardinal	2/1/2001	Clear	1.51886
Cardinal	3/1/2001	Clear	1.51866
Cardinal	4/1/2001	Clear	1.51870
Cardinal	5/1/2001	Clear	1.51875
Cardinal	6/1/2001	Clear	1.51885
Cardinal	7/1/2001	Clear	1.51857
Cardinal	8/1/2001	Clear	1.51876

3.1.2 Sample Set 2: Pilkington North America, Inc.

Sample set two is composed of 27 colorless float glass samples collected from September 2008 to April 2010. These samples were manufactured in Pilkington North America Inc. (Stockton, CA, USA). This plant underwent an Fe transition from high to low concentration from March 14, 2010 to March 19, 2010. The refractive indices of these samples were not determined as a result of previous research demonstrating the narrow spread of data. Table 3 summarizes sample set two.

Source	Sample Description	Color
Pilkington	9/24/08	Clear
Pilkington	10/12/08	Clear
Pilkington	12/28/08	Clear
Pilkington	12/26/08	Clear
Pilkington	1/4/09 B	Clear
Pilkington	1/4/09	Clear
Pilkington	4/26/09	Clear
Pilkington	6/16/09	Clear
Pilkington	7/24/09	Clear
Pilkington	8/17/09	Clear
Pilkington	9/06/09	Clear
Pilkington	10/4/09	Clear
Pilkington	11/15/09	Clear
Pilkington	12/19/09	Clear
Pilkington	1/24/10	Clear
Pilkington	1/31/10	Clear
Pilkington	2/7/10	Clear
Pilkington	2/14/10	Clear
Pilkington	2/18/10	Clear
Pilkington	2/25/10	Clear
Pilkington	3/3/10	Clear
Pilkington	3/14/10	Clear
Pilkington	3/19/10	Clear
Pilkington	3/26/10	Clear
Pilkington	4/2/10	Clear
Pilkington	4/16/10	Clear
Pilkington	4/9/10	Clear

Table 5. Sample Set 2, Pilkington North America, Inc.

3.2 Experimental Instrumentation and Procedure

The LIBS experiments were conducted on a home-built LIBS system. The system consisted of a New Wave Research Q-switched Nd:YAG Tempest laser (New Wave Research, Fremont, CA) operating at 266 nm, with a pulse width of 5 ns. Flashlamps and Q-switches were both externally triggered using a Berkeley Nucleonics delay generator (San Rafael, CA). The laser beam was expanded from ~4 mm to 12 mm using a Galilean telescope and focused at the normal incidence with a plano-convex lens with a focal distance of 150 mm. The laser remained at a constant energy of 27 mJ per laser pulse, producing a spot size of ~80 μ m. All analyses were conducted at atmospheric pressure with an argon sheath being delivered over the sample surface at 900 ml/min. Figure 22 displays a simple schematic of the LIBS system.

The plasma emissions were acquired at a 90° angle from the side using a pair of plano-convex lenses with a focal distance of 75 mm onto a 50 μ m diameter fiber optic cable. The fiber optic cable was coupled to an Andor Mechelle 5000 spectrometer equipped with an intensified CCD camera using a 1024 x 1024 chip. The collected spectral range was from 200-950 nm with a resolution of ~5000. The repetition rate for the spectrometer was 0.67 Hz.

To ensure representative sampling and to account for inherent glass heterogeneity, each glass sample was analyzed in replicates of five at different locations. Each replicate was the result of an accumulation of the last 50 laser pulses from a total 100 pulse replicates. To achieve the best reproducibility, highest signal-to-noise ratio, precision and accuracy, the lens-to-sample distance (LTSD), gate delay and integration time were

optimized. The laser was focused 1.3 mm into the sample surface, the optimized gate delay with respect to the laser pulse was $1.5 \ \mu s$ and the integration width was $12.0 \ \mu s$.



Figure 22. LIBS experimental setup schematic for forensic glass discrimination

Eighteen (18) emission lines corresponding to elements, Sr, K, Fe, Ca, Al, Ba, Na, Mg and Ti, were initially chosen because of their presence throughout the glass spectra. A typical float glass spectrum is seen in Figure 23. All emission peaks were background subtracted and the intensities were used for statistical analysis. If the precision for the stated elemental intensities were less 10% relative standard deviations (RSD) determined by the five replicates, the emission line was kept with the possibility of later being used in an elemental ratio for discrimination.





The first condition for the elemental ratio was to provide correct association with the positive controls, CRM 1831 and the two duplicate samples from within the set. The sample CRM 1831 was analyzed repeatedly throughout the analysis, the beginning, middle (at minimum once or every two hours) and end of the experimental procedure. Two randomly chosen duplicate float glass samples were analyzed at random time intervals. The duplicate samples and the CRM 1831 standard were required to be found indistinguishable from itself at all analysis times. Requiring duplicate samples to be indistinguishable excludes ratios that would result in a Type I error (false exclusion).The elemental ratios were constructed using all possible pairs [N(N-1)/2, N=number of samples]. The second condition when choosing an elemental ratio was the percent discrimination it provided within the float glass samples. Ten (10) discriminating elemental ratios were used in each sample set. The elemental ratios vary between sample sets to provide the highest possible discrimination.

3.3 Statistical Analysis

Pairwise comparisons were made using analysis of variance (ANOVA) and the General Linear Model (GLM) in Systat 11 (San Jose, Ca) with Tukey's honestly significant different test (HSD). The indistinguishable pairs produced by pairwise comparison analysis were then tested with a two sample t-test assuming unequal variances at a 95% confidence interval (Microsoft Excel, Redmond, WA). The samples found indistinguishable after the t-test were said to be indistinguishable, defined as having similar elemental profiles.

3.3.1 Discrimination Results LIBS: Cardinal Glass Industries

The Cardinal plant, sample set 1, had 49 samples producing 1176 possible pairs. The top 3 discriminating ratios were Al I 396.15/Ca I 534.95, K I 766.49/Na I 808.32 and K I 766.49/Ca I 616.22 discriminating 78.6%, 76.9% and 76.1% of the total possible pairs, respectively, while correctly associating duplicate samples and CRM 1831. All 10 discriminating ratios and their corresponding discrimination power are listed in Table 4.

For method validation, CRM 1831 was analyzed 6 times throughout the experimental procedure and all 6 times all the replicates were found to be indistinguishable when compared to the other 5 runs with the statistical analysis previously described. Two samples were chosen to be analyzed a second time in the experimental procedure. The randomly chosen duplicate samples were, 01/14/98b and 06/01/01b, and were used to assess for type I errors. Two sample pairs (01/14/98 & 01/14/98 b, 06/01/01 & 06/01/01 b) were found to be indistinguishable when compared with statistical analysis described above with the 10 discriminating elemental ratios.

Cardinal Ratios	% discrimination	Pairs discriminated
Al I 396.15/Ca I 534.95	78.6	924
K I 766.49/Na I 818.32	76.9	904
K I 766.49/Ca I 616.22	76.1	895
K I 766.49/Fe I 438.84	69.7	820
Sr II 407.77/Al I 396.15	67.8	798
Al I 394.40/Ba II 493.41	67.0	788
Al I 396.15/Na I 818.32	65.7	773
Fe I 371.64/Al I 394.40	61.4	722
Al I 394.40/Mg II 279.80	56.3	662
Sr I 460.73/Ca I 616.22	55.8	656

Table 6. LIBS Discriminating Ratios and the Percent Discrimination for Sample Set 1, Cardinal

Olass muustines	Glass	Industries
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Pairwise comparison discriminated 1119 pairs out of the 1176 possible pairs yielding a discrimination of 95.2%. Figure 24 shows the indistinguishable pairs by date. The x-axis and the y-axis are both labeled with the corresponding manufacturing dates and the dates range over the entire time of manufacture. Correlating a date on the y-axis with a date on the x-axis with provide the two dates of the pairs found to be indistinguishable. The two dates will then provide the time separation in manufacture. It is observed that the most similar elemental composition is within approximately 2 months of manufacture.



Figure 24. The indistinguishable pairs by ANOVA pairwise comparison using LIBS for sample set 1, Cardinal Glass Industries

Fifty (50) of the 57 indistinguishable pairs were discriminated by the t-test, producing a final discrimination of 99.4%. Of the 1176 combinations, LIBS produced no type I error and 7 remaining indistinguishable pairs. Table 5 lists the indistinguishable pairs. The 7 indistinguishable pairs ranged from 1 month (11/15/97 & 12/15/97, 03/15/99 & 04/14/99) apart to 15 months apart (03/15/99 & 06/01/01) in production time, with an average manufacture time separation of ~4 months.

Cardinal Glass I	ndustries
01/01/00 & 03/2	27/00
04/01/01 & 12/	01/00
03/01/01 & 08/	01/01
06/01/01 & 03/2	15/99
08/17/97 & 12/2	15/97
11/15/97 & 12/2	15/97
03/15/99 & 04/2	14/99

Table 7. Indistinguishable pairs by LIBS for Sample Set 1, Cardinal Glass Industries

Interpretation of indistinguishable automotive float glass pairs by previous research is vague. Bridge *et al.* ^{13,42} only reference the percent discrimination achieved with no details on actual sample dates and sources, i.e., make, model or year of car. Naes *et al.* and Schenk *et al.* ^{3,27} are clear with float glass sample descriptions and suggest indistinguishable pairs of float glass are a result of the glasses originating from the same source, i.e., both inside and outside windshield glass, on the basis of the glasses sharing a similar manufacturing date. However, as a result of this information not being readily available, the dates of float glass manufacture to vehicle installation are unknown. The current research demonstrates that it is possible for glass to have similar reoccurring elemental profiles over a time period ranging from 1-15 months, with the most similarities occurring within approximately 2 months of manufacturing date.

3.3.2 Discrimination Results LIBS: Pilkington North America, Inc.

The Fe transitioned from high to low concentration from March 14, 2010 to March 19, 2010. The elemental compositions of ingredients will vary as a result of the desired end

product. Iron is often varied in the manufacturing process, making it a good discriminating element. Iron is most often used to change the thermal emissivity of glass. Glass with low thermal emissivity values will not reflect thermal radiation, thereby increasing the transmittance.

Figure 25 demonstrates that LIBS is a sensitive analytical technique and is able to detect the differences in Fe concentration within a few days of production.





As a result of LIBS still being an invalidated technique in the forensic laboratory for the forensic analysis of glass, the LIBS results are compared to the well-established technique LA-ICP-MS for validation. The following chapter will cover LA-ICP-MS for the discrimination and association of float glass from a single manufacturing plant. The data for LA-ICP-MS is being compared here to demonstrate that LIBS is producing accurate data for the forensic analysis of glass.

Figure 26, seen below, illustrates that LIBS has a high correlation with LA-ICP-MS. The independent axis reports the concentrations of Fe produced by LA-ICP-MS during the transition period. The dependent axis is the background subtracted LIBS intensities. The Pearson's product-moment correlation coefficient produced a R² value of 0.992. The high value signifies that there is a high correlation produced between the relationship of the well-established LA-ICP-MS and LIBS, for the forensic analysis of glass.



Figure 26. Correlation between LIBS and LA-ICP-MS for the Fe transition at Pilkington North America Inc.

Illustrated in Figure 27 is the correlation of LIBS and LA-ICP-MS for the elemental profiling of Fe for all 21 glass samples. In order to represent the data of LA-ICP-MS and LIBS on the same set of axes, the LIBS signal was multiplied by 100 and the LA-ICP-MS concentrations were divided by a factor of 100.
Also observed in Figure 27, LIBS produces the same trend for signal intensities as does LA-ICP-MS for concentration of iron. The data represented illustrates the capability for LIBS to produce similar results as LA-ICP-MS data. Many forensic laboratories cannot not afford to acquire LA-ICP-MS instrumentation, in contrast, being less expensive, LIBS is proving to be an alternative elemental analysis technique.



Figure 27. The elemental profile of Fe for sample set 2 by LIBS and LA-ICP-MS The Pilkington plant, sample set 2, had 27 samples producing 351 possible pairs. The top 3 discriminating ratios were Fe I 438.84/Ti II 336.12, Fe I 438.84/Mg 517and Ca II 645.66/Ti I 365.35 discriminating 75.4%, 72.2% and 68.2 % of the total possible pairs, respectively, while correctly associating duplicate samples and CRM 1831. Table 6 lists all 10 discriminating ratios and their corresponding discrimination power.

Pilkington	%	Pairs
Ratios	discrimination	discriminated
Fe I 438.84/Ti II 336.12	75.4	265
Fe I 438.84/Mg 517	72.2	253
Ca II 645.66/Ti I 365.35	68.2	239
Sr 460/Ti I 365.35	68.0	239
Al I 394.40/Fe I 438.84	62.3	219
Fe I 438.84/Na I 330.13	61.1	215
Sr II 407.77/Fe I 438.84	60.3	212
Sr I 460.73/K I 766.49	50.2	176
Al I 396.15/Mg 280	44.6	157
K I 766.49/Na I 330.13	44.1	155

Table 8. LIBS Discriminating Ratios and the Percent Discrimination for Sample Set 2, Pilkington

North	America,	Inc
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The CRM 1831 was analyzed 3 times throughout the experimental procedure and no significance differences were determined. Two duplicate samples, 01/04/09b and 10/12/08b, were analyzed an extra time during the analysis. The pairs (01/04/09b & 01/04/09b & 10/12/08b & 10/12/08) were found to be indistinguishable when compared with statistical analysis using the 10 discriminating elemental ratios.

Pairwise comparison produced 111 indistinguishable pairs (240 distinguished), resulting in a 68.4% discrimination. The t-test further discriminated another 107 out of the 111 indistinguishable pairs, producing a discrimination of 98.8%. The remaining 4 indistinguishable pairs, see Table 7, range from only 2 weeks to 2 months apart.

Pilkington North America, Inc.
03/03/10 & 03/14/10
03/03/10 &02/07/10
10/12/08 & 12/28/08
01/31/10 &02/07/10

Table 9. Indistinguishable pairs by LIBS for Sample Set 2, Pilkington North America, Inc.

Overall, LIBS produced an average precision throughout the experiment in sample set one of ~6% RSD for all 490 combinations (10 ratios, 49 samples). The average precision in sample set 2 (270 combinations) was ~5% RSD throughout the entire experiment. The figures of merit for LIBS on CRM 1831 are list in Table 8, demonstrating the precision and accuracy of LIBS. The precision of LIBS can be as good as 1.5% RSD for K I 766.49 nm emission line and a bias of 1.0% for the Ba II 493.41 nm emission line.

	Conc.		Precision	%	LOD	LOQ
NIST 1831	(ppm)	SNR	% RSD	Bias	(ppm)	(ppm)
Al I 394.4	6381	277	2.5	2.0	70.7	235.6
Ba II 493.41	32	63	4.6	1.0	1.1	3.6
Sr I 460.73	89	285	4.0	3.6	0.9	2.9
Ca I 534.95	58604	1851	3.4	7.6	68.0	226.9
Fe I 438.44	802	40	3.1	16.0	21.0	70.1
K I 766.49	2738	1133	1.5	2.6	3.9	13.1
Mg II 279.80	21166	367	2.4	12.3	82.1	274.3
Na II 330.13	98825	1052	4.1		190.7	635.7

Table 10. LIBS Figures of Merit for CRM 1831

3.4 Round Robin Glass Studies

In efforts to standardize methods for the forensic analysis of glass, a grant by the National Institute of Justice was awarded to my mentor, Dr. Almirall. I was privileged to be able to participate in this working group as it consisted of both national and international analytical and forensic scientists. The working group provided me the opportunity to interact with working scientists.

The group was named the Elemental Analysis Working Group (EAWG) and to date I have been involved in five meetings. The objective of EAWG was to conduct elemental analysis of glass with different analytical techniques to improve the analytical method used for characterization and comparison, to evaluate the different statistical methods to determine match criteria, interpretation of these results and finally the reporting of these results. The group focused on LA-ICP-MS, ICP-MS, µXRF and LIBS. Only the LIBS portion of this working group will be compared, as my role was to represent FIU for the forensic analysis of glass using LIBS for four meetings that took place in August 2008, December 2009, August 2010 and December 2010, starting with round robin two.

It is important to note, that the first two inter-laboratory studies, FIU was the only LIBS laboratory, where in the fourth inter-laboratory study the LIBS participants increased to 5 laboratories, demonstrating the growth for LIBS as an analytical technique for the forensic analysis of glass.

Round robin two was an inter-laboratory study conducted on float glass standards NIST 1831, FGS 1 and FGS 2 to study the measurement variation and inter-laboratory

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variation¹⁶⁶. FGS 1 and FGS 2 are float glass standards produced by SCHOTT, Germany. These standards resemble soda-lime glass composition; however the elemental concentrations are different by a factor of 5. In addition to the float glass standards, an additional set of glass fragments were also analyzed. These second set of glass fragments were submitted for comparison to evaluate analytical results produced inter-laboratory.

The elemental analysis of glass results were separated into two groups. As a result of FIU being the only LIBS participant, LIBS was grouped with 7 XRF participants. In summary all participants in of this inter-laboratory study received instructions for analysis and the following glass samples with a given forensic scenario:

- 1) NIST 1831: Full thickness fragment
- 2) NIST 1831: small fragments
- 3) FGS 1: small glass fragments
- 4) FGS 2: small glass fragments
- 5) Item 1, known glass sample (K1): three glass fragments (2-7 mm) collected from broken window of victim's house.
- Item 2, question sample (Q1): three glass fragments (1-4 mm) recovered from the suspect's shirt.
- Item 3, question sample (Q2): three glass fragments (1-4 mm) collected from suspect's pants.

A likely crime scenario was provided and each participant was to associate or distinguish the known sample (K) to the questioned sample (Q). After results were submitted, it became known that K1 and Q1 samples were of the same origin, the two samples originated from the same glass pane. Sample Q2 had originated from a separate pane of glass produced from the same plant, manufactured ~3 years previously. All participants in group 1 and 2 correctly associated samples K1 with Q1 and discriminated K1 with Q2¹⁶⁶. The match criteria used for the XRF labs was spectra overlay with ± 2 or ± 3 standard deviations. The match criteria used for LIBS was ANOVA with student's t-test at a 95% confidence interval using elemental ratios Al/Sr, Fe/Sr, Ca/K, Al/Ca, Al/Na, Ba/Sr and Ca/Sr.

The accuracy and precision of the standard reference materials were also evaluated. However, as a result of FIU being the only LIBS laboratory, the interlaboratory accuracy/precision studies could not be compared. Different match criteria, as chosen independently by the analyst, all provided the correct results. In conclusion, this study indicated that LIBS is able to provide similar results as LA-ICP-MS and XRF.

Round robin three was composed of glass samples NIST 1831 and two glass sets. Set one was from the same manufacturing plant and was selected to study the capabilities of the different techniques to discriminate between different time intervals of glass production. This set consisted of 2 known samples and 3 questioned samples. The second set was to evaluate the elemental variation within container glass. As usual, all sample sets are distributed without the known associations provided. After results are submitted the association data is provided. This inter-laboratory study consisted of 1 ICP-MS, 5 LA-ICP-MS, 4 XRF and 2 LIBS laboratories. Unfortunately, as a result of the two LIBS method being very different, there could be no comparisons made between the two LIBS laboratories. However, a comparison of the analytical results of LIBS to both the established techniques of LA-ICP-MS and XRF are compared.

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All samples were previously analyzed by LA-ICP –MS and concentrations documented in the glass database at FIU. After analysis the results were provided that samples K2 versus Q1, K1 versus Q2 and K1 versus Q3, all have fairly distinct element profiles. Samples with similar elemental profiles were K2 versus Q1, K1 versus Q2, and K1 versus Q3. The dates of manufacture for the K and Q samples are listed in Table 9.

Database I.D.	Sample
8/17/2001	K1
8/31/2001	Q1
4/15/1998	K2
5/17/1998	Q2
7/17/1998	Q3

Table 11. Description of Sample Set One for Round Robin Three

Again a scenario was developed to mimic a potential crime scene. The LIBS results obtained are listed in Table 10 with the corresponding discriminating ratios. An "x" in the box signifies a significant difference between the elemental composition for that specified ratio.

x: different								
Summary	Na 818	K766	Fe438	Ca534	Al394	Al394	Sr460	Fe 438
systat	K 766	Ca 643	K766	K766	Sr460	Na330	K766	Al 396
K2 vs								
Q1	х	х	х	x	x	х	x	x
Q2	х		x	x	x	x	x	x
Q3	х		x	x			x	
x: different								
Summary	Na 818	K766	Fe438	Ca534	Al394	Al394	Sr460	Fe 438
systat	K 766	Ca 643	K766	K766	Sr460	Na330	K766	Al 396
K1 vs								
Q1								
Q2	х	х	x	x	x		x	
Q3	х	x	x	x	x	х	x	x

Table 12. LIBS Discriminating Ratios and Results for Round Robin Three

In the above table, K2 is found significantly different than all the questioned samples. K1 is found significantly different than Q2 and Q3, while no significant differences are produced between the elemental composition of K1 and Q1.

The inter-laboratory comparisons are best illustrated in the following Table 11¹⁶⁷ and Table 12¹⁶⁷ where K1 and K2 are compared to the questioned samples. H LIBS signifies my results.

Lab ID	K1 vs Q1	K1 vs Q2	K1 vs Q3	Match criteria
A XRF	IN	DS	DS	Spectra overlap
B XRF	IN	DS	DS	Spectra overlap, ± 3s of ratio intensities Ca/Mg, Ca/Ti Ca/Fe, Sr/Zr, Fe/Zr, Ca/K, Fe/Sr, Fe/Mn
C XRF	IN	DS	DS	Spectra overlap, ± 3s of ratio intensities Excluded by Ca/Ti, Ca/K. Ca/Mn
E XRF	IN	DS	DS	Spectra overlap, \pm 3s of ratio intensities
F XRF	IN	DS	DS	± 3s of ratio intensities Ca/Fe, Sr/Zr, Ca/K, Fe/Mn, Ca/Mn, Fe/Ti, Ca/Ti
H LIBS	IN	DS	DS	Elemental ratios, ANOVA + Tukey p=0.05
I LIBS	IN	IN^{*4}	DS	PLS algorithm
A ICP	IN*2	DS	DS	$\pm 2s$
B ICP	DS	DS	DS	$\pm 2s$ and $\pm 3s$
C ICP	DS	DS	DS	modified ±4s
D ICP	DS* ¹	DS	DS	t test (Bonferroni correction), p=0.05, *ANOVA + Tukey p=0.05
E ICP	IN * ²	DS	DS	t test p=0.05 and ANOVA (p=0.05)
F ICP	IN* ²	DS	IC *3	Range overlap and $\pm 3s$
H ICP	DS	DS	DS	modified ±4s

Table 13. Final Round Robin 3 Report, Comparison of K1 to Questioned Samples¹⁶⁷

In the above Table 11, the following notations and definitions signify: IN: samples are indistinguishable, DS: samples are distinguishable, IC: inconclusive, *: sample Q3 suffer problems during digestion, therefore the precision does not allow a fair comparison, *2: participant reported indistinguishable, but t-test of raw data shows significant differences on some elements¹⁶⁷.

The K1 versus Q1 samples are manufactured approximately two weeks apart, therefore it is assumed that their elemental composition would be similar as a result of previous conducted studies. It is observed that only 4 LA-ICP-MS laboratories and I, using LIBS, found these samples to be distinguished. This sample pair was distinguished by the Na/K ratio, where most ICP labs found Ba to be one of the most discriminating elements.

The K1 versus Q2 and K1 and Q3 samples were found to be distinguishable by most all laboratories. These results were expected, as a result of previously conducted research, that these two sample pairs would have a distinct elemental profiles as a result of their manufacturing time being a difference of approximately 3 years.

Lab ID	K2 vs Q1	K2 vs Q2	K2 vs Q3	Match criteria
A XRF	DS	DS	IN	Spectra overlap
B XRF	DS	DS	IN	Spectra overlap, ± 3s of ratio intensities Ca/Mg, Ca/Ti Ca/Fe, Sr/Zr, Fe/Zr, Ca/K, Fe/Sr, Fe/Mn
C XRF	DS	IN	IN	Spectra overlap, ± 3s of ratio intensities Excluded by Ca/Ti, Ca/K. Ca/Mn
E XRF	DS	IN	IN	Spectra overlap, \pm 3s of ratio intensities
F XRF	DS	DS	IN	± 3s of ratio intensities Ca/Fe, Sr/Zr, Ca/K, Fe/Mn, Ca/Mn, Fe/Ti, Ca/Ti
H LIBS	DS	DS	DS	Elemental ratios, ANOVA + Tukey p=0.05

Table 14. Final Round Robin 3 Report, Comparison of K2 to Questioned Samples¹⁶⁷

I LIBS	DS	DS	IN	PLS algorithm
A ICP	DS	DS	IN ^{*2}	± 2s (for 10 elements menu, if number of overlaps 9 or 10 then match if <9 then non- match)
B ICP	DS	DS	DS	$\pm 2s$ and $\pm 3s$
C ICP	DS	DS	DS	modified ±4s
D ICP	DS	DS	DS	t test (Bonferroni correction, p=0.05), ANOVA + Tukey, p=0.05
E ICP	DS	DS	IN ^{*2}	t test at 95% and ANOVA (95%)
F ICP	DS	DS	IC *	Range overlap and $\pm 3s$
Н ІСР	DS	DS	DS	modified ±4s

In the above Table 12¹⁶⁷, the following notations and definitions signify: IN: samples are indistinguishable, DS: samples are distinguishable, IC: inconclusive,*: sample Q3 suffer problems during digestion, therefore the precision does not allow a fair comparison, *2: participant reported indistinguishable, but t-test of raw data shows significant differences on some elements¹⁶⁷.

The K2 versus Q1 and K2 versus Q2 samples are manufactured approximately 3 years apart and are found distinguishable by most laboratories. The K2 versus Q2 samples are found indistinguishable by two XRF laboratories. Sample pair K2 and Q3 were manufactured 3 months apart. All XRF participants and the other LIBS participant found these samples to be indistinguishable. These results demonstrate that LIBS may provide more sensitivity than the well-established analytical method XRF and competes as an analytical method for the forensic analysis of glass against LA-ICP-MS when operated under optimized conditions.

Sample set two in round robin two was a green Perrier water bottle that was broken and the glass fragments were analyzed, see Figure 28.



Figure 28. Sample Set 2, Perrier bottle, for round robin three

Five fragments from the bottle were sampled to study the homogeneity. Samples B1, B2 and B3 were all taken from the center of the bottle, B4 from the lower portion and B5 was taken from the bottle neck. The following Table 13 demonstrates the discriminating ratios used for analysis.

It has been documented that the elemental composition in container glass has greater heterogeneity than float glass⁴¹. The heterogeneity is often contributed the manufacturing process as a result of the molding parts providing contamination⁴¹. In previous research by Trejos *et al.* it was reported that the inherent variation within the elemental composition of the container is greater than the instrumental variation using LA-ICP-MS⁴¹.

X=different							
	Ca534	AI396	Al394	Al394	AI394	Na330	Ca645
Summary systat	Sr460	Ca534	Sr460	Ca534	Fe438	Si288	Mg 279
B1							
B2			Х		X		
B3							
B4							
B5							

Table 15. Round Robin Three Perrier Bottle Analyses

To evaluate the variation between the different analytical techniques, all statistical analyses were done in the same manner using ANOVA, followed by a t-test at a 95% confidence interval. The LIBS data I produced found significant differences between pairs B2 and B4 with the elemental ratio Al/Sr and between pair B3 and B2 with elemental ratio Al/Fe, see Table 13.

All participants found significant differences between the container set except for solution ICP-MS where the total mass samples is milligrams compared to LIBS consuming nanograms to micrograms. The results obtained here demonstrate that more samples need to be analyzed to produce an accurate elemental profile for container glass for all micro-sampling techniques.

The final round robin for which I participated in concentrated on statistical analysis from round robin 3 and round robin 4 to evaluate the effect on type I and type II errors¹⁶⁸. The sample set of round robin 4 was also from a single manufacturing plant. This set consisted of 2 known glass fragments and 3 questioned samples. Round Robin 4 had 3 participants report results using LIBS.

All participants performed the following statistical tests for match criteria for data from round robin 3 and round robin 4: 1) range overlap, 2) t-test at 99% confidence

interval, 3) t-test at a 95% confidence interval, 4) t-test with Bonferoni correction, $5) \pm 2$ standard deviation, 6) ± 3 standard deviation, 7) ± 4 standard deviation and 8) Hotelings T.

Using the FIU glass database, sample pairs for round robin 4 with similar elemental composition were K2 versus Q1. Sample Q1 was manufactured on 02/18/2010 while all other samples, K1, K2, Q2 and Q3 all originated from the same date, 03/03/2010. The known fragments were provided to participants at full size, meaning there was original surface of both the float and non-float side, and the questioned samples were provided as irregular fragments (0.5-1 mm).



Figure 29. Glass fragments provided for round robin four

To provide reproducible results for LIBS analysis the glass fragments were mounted in a soft modeling compound, orientated so that a flat non-float surface can be ablated, see Figure 29. Figure 29a is sample K1, it is evident, that even as a full thickness fragment, it is still very small. Figure 29b is sample Q1. Care needed to be given to all samples, so that there would be space for 5 replicates with a laser spot size of ~100 μ m for LIBS analysis.

First, all participants provided results using their selected match criteria. All participants responded correctly and found Q1 to be distinguishable samples from K1 and K2. I was the only LIBS participant to correctly report that Q1 to be distinguished from samples K1 and K2. This is explained as the glass method I have developed has been optimized and validated with FIU LIBS instrumentation.

Unfortunately, the LIBS data varied greatly between laboratories. The lack of standardization inter-laboratory using LIBS, such as; instrument laser wavelength, temporal parameters and data treatment, produced a large variation in LIBS results. LIBS, still being a novel technique for the forensic analysis of glass, is not yet standardized within the LIBS community resulting in inter-laboratory inconsistency. More studies need to be conducted with LIBS before a match criteria can be suggested.

Match criteria methods were focused on for ICP and XRF techniques as a result of having method standardization. It was determined that match criteria needs to be selected with care based on elemental technique used. Analytical instrumentation achieving precision of $\leq 2\%$ RSD may be too sensitive and produce false exclusions for match criteria using the t-test. The false exclusion rate was significantly reduced by using a 3% RSD and a match criteria of ±4 standard deviations¹⁶⁸.

3.5 Conclusions

Laser induced breakdown spectroscopy was shown to be a powerful and sensitive technique for the forensic association and discrimination of float glass. The elemental concentrations of float glass varies during the manufacturing process. These variations provide discrimination of float glass samples within the same manufacturing plants from days to years apart. LIBS has the ability to detect the small variations within the elemental profile. Eighteen (18) emission lines corresponding to the elements Sr, K, Fe, Ca, Al, Ba, Na, Mg and Ti, were chosen because of their detection above the method detection limits and for presenting differences between the samples. The elemental ratios producing the most discrimination in the first sample set, Cardinal Glass Industries, were; A1 I (396.15)/Ca I (534.95), K I (766.49)/Na I (808.32) and K I (766.49)/Ca I (616.22) discriminating 78.6%, 76.9% and 76.1%, respectively, of the possible 1176 pairs. The elemental ratios producing the most discrimination in the second sample set, Pilkington North America, Inc., were; Fe I (438.84)/Ti II (336.12), Fe I (438.84)/Mg I (517.27) and Ca II (645.66)/Ti I (365.35) discriminating 75.4%, 72.2% and 68.2% respectively, of the possible 351 pairs. When all the ratios are combined in a comparison, 99% of the possible pairs were discriminated from two different float glass sample sets manufactured from a day to years apart, using the optimized LIBS method. LIBS achieved good precision (~5% RSD) throughout both studies. These results support the hypothesis that the elemental composition of glass produced in a single plant over time varies more than the differences that can be detected using analytical LIBS. The robustness of this technique is demonstrated with the production of no type I errors.

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The present research demonstrated that similar elemental profiles are possible from 1-15 months apart. However, data supports the most similar elemental profile being within 1-3 months of manufacture.

The LODs achieved by LIBS are below the expected ranges encountered in the elemental concentration of float glass, making LIBS a fit technique for the forensic analysis of glass. LIBS demonstrates to compete with well-established methods of LA-ICP-MS and XRF for the forensic analysis of glass. However, if LIBS is to be the next analytical method found commonly in the forensic laboratory, standardization of instrumentation, methodology and match criteria need to be assessed.

4 Laser Ablation Inductively Coupled Mass Spectrometry for the

Discrimination and Association of Float Glass from Single Manufacturing Plants

Previous conducted research documents the discrimination between float glass ^{14,169-173}. Bridge *et al.* ¹⁶⁹ analyzed 27 float glass samples originating side window and side mirror glass collected from automobiles. These authors report a 74% discrimination using LA-ICP-MS. However, Naes *et al.* demonstrate that 99% of the automotive samples from within the same car can be discriminated ranging in year from 1998 to 2004. The author's state that the 1% of indistinguishable pairs are explained by the pairs originating from the same vehicle and that this is a result of the float glass having been manufactured at the same plant at approximately the same time ¹⁷⁰. To date, however, no studies have reported the association and discrimination of float glass from a single plant in such short periods of time with LA-ICP-MS. The next section focuses on the capability for LA-ICP-MS to discriminate float glass produced at the same plant at approximately the same time

4.1 Glass Sample Set for LA-ICP-MS

The sample set composed of 27 colorless float glass samples collected from September 2008 to April 2010. These samples were manufactured in Pilkington North America Inc. (Stockton, CA, USA). The refractive indices of these samples were not determined due to previous research demonstrating the narrow spread of data. Table 3 summarizes sample set two. This is the same set as analyzed previously with LIBS.

4.2 LA-ICP-MS Experimental Instrumentation for Glass Analysis

All samples were examined on the non-float surfaces of the respective glass. Float glass certified reference material (CRM) NIST 1831 was included into the experimental procedure as an internal control to determine accuracy, because of the similar matrix.

All glass analysis was conducted on a quadrupole ELAN DRC II (Perkin Elmer, Shelton, CT, USA) to a 213 nm 4 nanosecond Q-switched Nd:YAG laser (NewWave Research, Fremont, CA, USA). The laser was operated at a fluence of 27 J/cm², with a spot size of 55 μ m, a repetition rate of 10 Hz, a 60 second dwell time and single spot ablation. Helium gas, at flow rate of 0.9 L/min, was the carrier gas from the sample chamber which blended with argon, the makeup gas, at 1 L/min before introduction into the ICP. The RF power of the ICP was set to 1500 W, with the plasma is being sustained with an argon flow of 16 L/min.

4.3 Statistical Analysis

The LA-ICP-MS analyses of the glass samples were performed following the NITECRIME (Natural Isotopes and Trace Elements in Criminalistics and Environmental Forensics) method ¹⁷⁴. The isotopic elemental menu was comprised of ⁷Li, ²⁵Mg, ²⁷Al, ²⁹Si, ³⁹K, ⁴²Ca, ⁴⁹Ti, ⁵⁵Mn, ⁵⁷Fe, ⁸⁵Rb, ⁸⁸Sr, ⁹⁰Zr, ¹¹⁸Sn, ¹³⁷Ba, ¹³⁹La, ¹⁴⁰Ce, ¹⁴⁶Nd, ¹⁷⁸Hf, ²⁰⁶Pb, ²⁰⁷Pb, and ²⁰⁸Pb. The CRM NIST 612 glass was used as an external calibrator and ²⁹Si was used as the internal standard. The CRM NIST 612 glass was analyzed at the beginning, end and throughout the experiment to account for drift over the time of the analysis. All glass samples were analyzed 3-4 times at different locations to ensure representative sampling and to account for any inherent sample heterogeneity.

The integrated signal was background subtracted and Glitter Software (GEMOC v4.4, Macquarie University, Australia) was used to determine the concentration of the elements. Data analysis was done with analysis of variance (ANOVA) pairwise comparisons with the General Linear Model (GLM) with Tukeys's honestly significant different test (HSD) using Systat 11 data analysis software (San Jose, CA). T-tests using Microsoft Excel (Microsoft, Redmond, WA) at a 95% confidence interval were performed to glass samples found indistinguishable, having very similar elemental profiles.

4.4 Discrimination Results

The sample set produced 351 possible pairs. Two duplicate samples were analyzed at random times during the analysis for method validation. The duplicate samples were positive controls and were required to be indistinguishable from itself. The glass standard NIST 1831 was used to determine accuracy.

Float glass samples ranged from years apart to days apart. As predicted the float glass samples that were further apart in manufacturing date produced a greater variation in their elemental profile. All possible pairs were discriminated from one another except for the two positive controls, which were found indistinguishable by the elemental menu. Table 14 provides a list of the top discriminating isotopes and the percent each isotope distinguished. The highest discriminating elements in this sample set were Ti, Fe and Zr.

Table 16. LA-ICP-MS Discriminating I	lsotopes and	Percent Discr	imination for	Pilkington
Amer	rica Inc.			

Element	# pairs	% discriminated
⁴⁹ Ti	325	92.6
57 Fe	282	80.3
⁹⁰ Zr	281	80.1
³⁹ K	242	68.9
⁸⁸ Sr	223	63.5
55 Mn	206	58.7
Al	108	30.8
178 Hf	33	9.4
137 Ba	26	7.4
25 Mg	7	2.0
140 Ce	4	1.1

Generally stating, the further apart in time float glass is manufactured, the greater the variability is witnessed in the elemental profile. For example, pair 12-28-08 and 02-14-10 were manufactured \sim 1 year apart and differed by 4 elements: Ti, Mn, Sr and Ba. Pairs manufactured within the same month (02/07/10, 02/14/10, 02/18/10 and 02/25/10) differed from one to three elements. Pairs 02/14/10 and 02/18/10 manufactured four days apart vary only in Sr and Ti concentration.

Table 15 lists the excel output for a t-test assuming unequal variances for sample pairs 12/26/08 and 12/28/08 which were manufactured 2 days apart and vary by only one element, Ti. Table 15 also lists the excel output for two duplicate samples, P031910 and PD031910 which were analyzed at random times throughout the experimental procedure. The t-tests were conducted at a 95% confidence interval. Defining the null as hypothesis as there is no significant difference, if the P value is greater than 0.05, the null hypothesis is accepted. Sample pairs P031910 and PD031910 produce a P value of approximately 0.41, concluding that there is no significant difference between these two samples. The results validate that the method is producing no Type I errors, false exclusions.

Sample pairs 12/26/08 and 12/28/08 produced a P value of 0.0007. With a P value less than 0.05 the null hypothesis is rejected and these two samples are found to be significantly different. The element concentration for Ti determined by LA-ICP-MS was 952.57±20.64 ppm (RSD 2.17%) and 862.25±12.89 (RSD 1.50%) for 12/26/08 and 12/28/08, respectively. These concentrations are close to one another, demonstrating that a sensitive, analytical technique is needed for the forensic discrimination of glass.

49Ti	P031910	PD031910	⁴⁹ Ti	P122608	P122808
Mean	284.56	278.40	Mean	952.57	862.25
Std. Dev.	11.3	7.6	Std. Dev.	20.6	12.8
Observations	4	4	Observations	4	4
df	5		df	5	
t Stat	0.91		t Stat	7.42	
P(T<=t)			P(T<=t)		
two-tail	0.4065		two-tail	0.0007	
t Critical two-			t Critical two-		
tail	2.57		tail	2.57	

Table 17. Excel Output for T-test Assuming Unequal Variances for Duplicate and Sample Pairs

Manufactured Two Days Apart

It is possible that glass fragments originating from the same source can be discriminated as a result of the difference in precision of measurement of the instrumentation and precision of the glass pane. For example, if the precision of the measurement for a given fragment is smaller than the overall precision of elemental concentrations within the glass pane, the sample would be discriminated. Therefore, it is important that the forensic examiner provides a representative characterization of the elemental profile to account for the homogeneity/heterogeneity of the glass pane to prevent incorrect associations or discriminations.

4.5 Conclusions

LA-ICP-MS is shown to be a sensitive analytical method for the forensic association and discrimination of float glass. The temporal variation in the elemental concentration of float glass within a single manufacturing plant was determined for the first time. The variations of these elemental profiles provide 100% discrimination of samples within the manufacturing plant.

Variations in the trace and minor elements, Zr, Sr, Mn, Fe and Ti, produced the greatest power of discrimination. The results of this study corroborate previous studies that report float glass samples from different manufacturing plants are significantly different by chemical composition and can be discriminated by many elements. The elemental composition of float glass originating from a single manufacturing plant is most similar within a month's production time. Greater variability in the elemental profile is observed in single plant production, as the manufacture dates increase in time. The greatest variability is observed between different float glass manufacturers.

5 Quantitative Analysis of Liquids from Aerosols and Microdrops using Laser Induced Breakdown Spectroscopy

Inkjet printing will be used to deliver to deliver small sub-nanoliter volume solutions with known absolute mass loadings for LIBS analysis. Inkjet printing is a contactless method for depositing precise volumes of solutions and able to deliver drops ranging from a few microns in diameter to tenths of a millimeter⁶², depending on the nozzle orifice.

It is the motivation of this research to use LIBS to accurately and precisely analyze small volumes of solution, \leq 300 µL for aerosol analysis and 90 pL for singlemicrodrops. These two methods eliminate the splashing and the sample preparation steps that have been reported for previous LIBS solution methods, as well as dramatically reduce the total volume needed for analysis.

5.1 The LIBS Instrumentation

A schematic of the LIBS instrumentation can be seen in Figure 30. The LIBS system was constructed using a Solo Nd:YAG PIV dual head laser (New Wave Research, Freemont California, USA) operated at 532 nm for single-pulse and collinear double-pulse experiments for aerosol and single microdrop in air. Microdrop LIBS on the aluminum stub utilized a 266 nm Tempest Laser (New Wave Research, Freemont California, USA). Pulse widths of both laser systems were 3-5 ns full width half-maximum with a beam diameter of approximately 4 mm exiting the laser head. Flashlamps and Q-switches were both externally controlled by a Berkeley Nucleonics (San Rafael, California, USA) pulse/delay generator model 575. A Galilean telescope was used to enlarge the beams approximately three times to 12 mm and were then focused to a spot size ~85 μ m for aerosol and microdrop in air and ~215 μ m for microdrops on an aluminum stub, through a plano-convex lens with a focal length of 150 mm. The LIBS optical emissions were collected and imaged at a 90 degree angle from the plasma using a pair of plano-convex lenses with a focal distance of 75 mm onto a 50 μ m fiber optic cable that was coupled to the entrance slit of an AndorMechelle 5000 spectrometer equipped with an Ando iStar intensified CCD camera using a 1024 x 1024 chip (Andor Technology, South Windsor, CT, USA). Solis software (Andor Technology) was used to control the gate delay, gate width and integration time. Five replicates were analyzed and averaged for the calculations.



Figure 30. Schematic of a) Microdrop LIBS in air or b) Aerosol LIBS experimental set-up

5.2 LIBS Optimization for Aerosol and Microdrop analysis

Optimum gate delays and gate widths depended on the emission line, sample matrix, laser fluence, and the ambient atmosphere. Temporally resolved measurements are evaluated to enhance the emissions lines of the LIBS spectrum. As vast amount of research has been done on temporal gating¹⁷⁵⁻¹⁷⁸ and by utilizing the different relaxation times between lines, spectral interferences may be minimized¹⁷⁹. Laser energies, gate widths, gate delays (respective to laser pulse) and the interpulse delay were optimized for highest signal-to-noise, corresponding to the best precision and accuracy. It is the goal of the optimization studies to produce the highest emission intensities for the desired analyte. As a result of all optimization studies being conducted with similar experimental procedure, repetition is avoided by only illustrating particular studies.

The plasma is formed within nanoseconds after the pulse but the detector reading is delayed approximately 1 μ s, thereby allowing the continuum to decay. The continuum is primarily because of the Bremsstrahlung process in which is dominated by photons emitted by electrons ⁷² and this process decays more quickly with time than the spectral lines. For the current work, the plasma was viewed from sequential gate delay times ranging from 1 μ s to 3.5 μ s with a constant acquisition time of 10 μ s.

Figure 31 illustrates a linear relationship between the gate delay time and the intensity values. The longer the gate delay the less spectral emission is detected.



Figure 31. Optimization of gate delay for a) Aerosol and b) Microdrop LIBS in air A gate delay of 1.75 µs in both aerosol and microdrop LIBS was determined to provide the best precision with maximum intensity, after background subtraction. It is at this point that the light is collected, transferred and detected. Each element has an exclusive emission spectrum; the wavelength corresponding to the emission line.

A precision of \sim 5% RSD was obtained in aerosol LIBS for gate delays between 1.75 and 3.50 µs, while a gate delay of 1 µs produced a precision of 9%RSD. The precision in microdrop LIBS was not as good as aerosol LIBS. The average precision

was \sim 13% RSD. Both configurations had worse precision at the 1 µs time delay. This is attributed to the continuum still being dominant and not having achieved local thermodynamic equilibrium.

Detector observation times (gate width) vary greatly from nanoseconds to hundreds of microseconds, depending on the application, matrix and laser energy. There are different rates of decay for the continuum and the analyte species. Below in Figure 32 is an example of the optimization for the detector observation time for collinear doublepulse LIBS.



Figure 32. Optimization of integration time for double-pulse microdrop LIBS

It is observed in this figure that the intensity does not increase significantly after 10 μ s. The integration time of 10 μ s was determined to be the optimized value.

For the current work, a constant high signal corresponding to the best sensitivity and repeatability was found at an observation time of 8.75μ s for double-pulse and 6.75μ s for single-pulse with an average precision in the double-pulse configuration of 3.5% RSD for aerosol LIBS. Microdrop LIBS observation times were 7 µs for single-pulse and 10µs for double-pulse corresponding to a 14% RSD for microdrop LIBS. It has been noted that conventional single-pulse LIBS is less sensitive than the competing atomic spectroscopic technique of ICP-OES that utilizes a sustained plasma as the excitation source but also requires much more analytical volume. In an effort to increase the LIBS sensitivity, double-pulse LIBS excitation is explored. Different laser pulse configurations have contributed to improving the limits of detection (LOD), by increasing the LIBS signal^{63,64}. Double-pulse LIBS techniques use a combination of two lasers or two pulses from one laser. Both are spatially overlapped and the two laser pulses are focused and separated by an optimized time ranging from nanoseconds to tens of microseconds separation.

The current work in aerosol and microdrop LIBS uses a collinear double-pulse configuration (as opposed to an orthogonal configuration). In the collinear configuration the two laser pulses propagate sequentially along the same axis and are focused onto the same location on the sample. Collinear double-pulse LIBS leads to increased mass ablation and the reheating of the plasma with the second pulse producing a longer-lived plasma than the single-pulse, increasing the analytical signal^{63,64}. The separation of the two laser pulses was optimized for the highest increase in analytical signal. Figure 33 for microdrop LIBS illustrates the analytical signal trend for an interpulse laser delay ranging from zero to 3000 nanoseconds.



Figure 33. Collinear interpulse delay optimization in aerosol LIBS for Sr II 407.7 nm The lowest point on the graph at time delay zero is for single-pulse LIBS and it produced a background subtracted intensity of 5285 counts. The mid-point on the graph at time delay of zero is the time when both pulses are being delivered with no delay; this produced an intensity of 13053 counts. The highest point in the graph is at 100 ns with a produced intensity value of 16002 counts. This was a preliminary study to observe the trend of collinear pulse in an aqueous environment, to determine approximately when the greatest intensity increase is observed. A further study was then conducted with microdrop LIBS to focus in on the exact optimized delay.

The collinear interpulse delay is optimized for the highest emission signal and best precision for the elements of interest. Figure 34 illustrates the correlation of intensity with interpulse delay in intervals of 50 ns for four different emission lines. It is observed that at greater delay times the plasma density decreases with the gate width held constant. Each elemental emission line has two points on the y-axis at time zero. The lower point is single-pulse LIBS and the higher point is both lasers firing at the same time with no interpulse delay. The same trend as previously was observed, however, the highest analytical signal was observed at an interpulse delay of 50 ns. The highest increase observed for emission lines Sr II 421.55 nm, Mg II 280.27 nm, Ba II 455.40 nm and Ca 396.85nm was during the interpulse delay time of 50 ns. Both aerosol and microdrop LIBS produced similar results, with the greatest increase in analytical signal corresponding to an interpulse delay of 50 ns.



Figure 34. Collinear interpulse delay optimization in microdrop LIBS for Sr II 421.5 nm, Mg II 280.2 nm, Ba II 455.5 nm and Ca II 396.8 nm

Argon has been demonstrated to increase the LIBS signal by producing a higher plasma temperature and higher electron density, resulting in higher emission intensity. Iida demonstrated that the plasma decay was reduced in an argon environment because of its low thermal conductivity¹⁸⁰. Wisbrun *et al.* demonstrated that an argon atmosphere produced almost doubled the intensity values and provided better precision. This was contributed to argon protecting the excited atoms from forming more stable compounds, such as oxides.¹⁸¹ Argon was used as the carrier gas at a constant flow of 700 mL/min to

transport the solution that was converted to a fine aerosol by a commercial nebulizer (ESI, Omaha, NE, USA) designed for ICP systems with a flow rate of 40 μ L/min. Figure 35 shows the optimization studies for the flow of Argon.



Figure 35. Optimized argon flow rate for aerosol LIBS for a) Mg II 279.5 and b) Sr II 407.7 nm It is observed that there is a linear relationship between argon flow rates and intensity between the flows of 400 and 700 mL/min. The flow rate of 700 mL/min was chosen as it provided the highest analytical signal.

In conclusion, the optimized parameters, for single-pulse aerosol LIBS were a laser wavelength of 532 nm, laser energy at 65 mJ, a gate delay of $1.75 \ \mu$ s, a gate width

of 6.75 μ s and an argon flow of 700 mL/min. Double-pulse aerosol LIBS parameters had both pulses delivered at 65 mJ, with an interpulse delay of 50 ns, a gate width of 8.75 μ s and all other settings remained unchanged.

The optimized parameters for single pulse microdrop LIBS on an aluminum stub were a laser wavelength of 266 nm, a gate delay of $1.1 \,\mu$ s, a gate width of 5.75 seconds and a frequency of 0.66 Hz.

The optimized parameters for single-pulse and collinear double-pulse microdrop LIBS experiments were, for single-pulse: a laser wavelength of 532 nm, a laser energy for 35 mJ per pulse, an argon sheath over the LIBS plasma delivered at 300 ml/min with 10 mm inner diameter tubing positioned 60 mm from the LIBS plasma, a gate delay of 1.75 μ s (respective to laser pulse), gate width of 7 μ s, a frequency of 0.66 Hz. Collinear double-pulse parameters consisted of both pulses at 35 mJ, with an interpulse delay of 50 ns and a gate width of 10 μ s, while all other parameters remained constant. Precision and accuracy was measured by 5 replicate measurements on all samples.

5.2 Aerosol LIBS Experimental Instrumentation

An injector tube, typically used for the torch of an ICP-MS, was attached to the flow chamber and produced a fine aerosol mist. The laser was focused ~2 mm from the injector orifice, where the effluent was introduced into the LIBS plasma. Figure 36 is a photograph taken during an aerosol LIBS event. At the tip of the injector, the LIBS plasma ionizes the effluent from the injector.



Figure 36. Experimental aerosol LIBS setup

The LIBS signal is then collected from the side with the collection optics where the signal is then transformed and output onto the computer.

Single-pulse and collinear double-pulse experiments were achieved with a 20 shot accumulation at a frequency of 0.66 Hz, which equates to a 30 second analysis time, and an absolute volume of 20 μ L being consumed per analysis.

Multi-element calibration standards were prepared from stock 1000 and 10,000 ppm solutions and made into concentrations ranging from 0 to 3000 ppm. For aerosol LIBS, the multi-element solutions containing Ca, Ba, Sr and Mg were prepared with final concentrations of 0, 5, 7.5, 15, 25, 50, 125, and 250 ppm. Continuing calibration

verification standards (CCVs) were prepared independently and used for method validation and to quantify bias at 25 ppm for aerosol analysis. The CCVs were analyzed randomly throughout the experimental procedure.

5.3 Aerosol LIBS Data

For aerosol LIBS, the use of the spray chamber created uniform sized droplets producing better precision. The ejected particles are captured by the plasma. Images acquired using a PI-MAX nanosecond gated camera (Princeton Instruments, Acton, MA, USA) suggests that not all the effluent exiting the injector was being consumed. The plasma is capturing a only certain percentage of the particles ejected by the LIBS plasma, Figure 37.



Figure 37. Aerosol LIBS effluent exiting the orifice into LIBS plasma

However, it is expected that a consistent aerosol volume (and analyte mass) of the effluent is consumed within each LIBS plasma formation. Aerosol LIBS analysis consumed less than 300 μ L of total sample volume during the accumulation of 20 laser pulses per replicate for a total of 5 replicates measurements per sample.

5.3.1 Aerosol LIBS: Single-pulse and Double-pulse quantitative analysisA single-pulse LIBS spectra in Figure 38 illustrates linearly increasing emission lineintensities with increasing concentration, indicating LIBS that is capable of quantitative analysis.


Figure 38. Single-pulse aerosol LIBS spectra for concentrations ranging from 0-250 ppm In the SP aerosol LIBS spectra seen in Figure 38, it is observed that at a concentration of 7.5 ppm, the LOD is approached. Figure 39, seen below, is a double-pulse aerosol LIBS spectrum for 1 ppm and a very nice narrow peak is produced, illustrating the increase in analytical signal, hence lowering the LOD.

The signal enhancements are more pronounced for emission lines with higher excitation energy levels and this observation has previously been reported by others^{177,178}. In aerosol LIBS, the sensitivity for the Ca II 396.85 nm emission line, total analytical volume of ~20 μ L of a 50 ppm solution (~ 1 μ g of mass),produced an increase of signal-to-noise ratio from 42 in the single-pulse configuration to 62 in double-pulse while improving the precision from 5.2% RSD to 0.5% RSD.



Figure 39. Double-pulse aerosol LIBS spectra of Sr II 407.7nm emission line at a concentration of 1 ppm and blank solution

Previous research has defined the excitation energy level for ionic lines as the sum of the ionization energy and the upper energy level^{177,182}. The excitation energy for Ba II 455.40 nm, Sr II 421.5 nm, Ca II 396.9 nm and Mg II 280.3 nm are 7.9, 8.6, 9.2, and 12.1 eV, respectively. The maximum enhancement in collinear double-pulse LIBS was observed at a 50 ns interpulse delay. The observed enhancements in aerosol LIBS were a multiple of 1.5, 1.6, 1.7 and 2.5 as compared to a single-pulse for Ba II 455.40 nm, Sr II 421.55 nm, Ca 396.85 nm and Mg II 280.27 nm, respectively, suggesting that the signal enhancements are larger for ionic lines with higher excitation energies.

A calibration of the response versus the concentration was constructed to conduct quantitative analysis for aerosol LIBS. Multi-element solutions containing Ca, Ba, Sr and Mg with final concentrations of 0, 5, 7.5, 15, 25, 50, 125, and 250 ppm were used.

Figure 40 illustrates calibration curves for Mg and Ba emission lines by single-pulse aerosol LIBS.



Figure 40. Aerosol LIBS calibration curves for a) Mg II 279.5 and 280.2 nm b) Ba II 493.4 and 455.5 nm emission lines

As a result of the homoscedasticity of the data, unweighted calibration curves were created for single-pulse and double-pulse LIBS. The LIBS signal response to a known mass concentration was established with good linearity ($R^2>0.99$) for both single and double-pulse configurations. All points on the calibration curves of the different emission lines were reproducible with typical precision of 2-6% RSD. Aerosol LIBS produced better sensitivity for the double-pulse versus the single-pulse configuration. The LOD for Sr II 421.5 nm decreased from 3.3 ppm to 1.0 ppm and Mg II 279.5 decreased from a LOD of 2.6 in single-pulse compared to 0.3 ppm in double-pulse. Ba II 493.4 nm and Ca II 396.3 nm produces LODs of 0.7 ppm and 0.6 ppm, respectively.

The flow of the nebulizer at 6.67 x 10^{-7} µL/µs provided a total analytical volume of 20µL being consumed during the 20 laser pulse analysis. The total mass delivered within the 20 µL sample volume at a sample concentration of 25 ppm is 0.05 µg. With a spectral viewing time totaling 175 µs, the volume introduced into the plasma during the observation is equivalent to an absolute mass of 2.92 pg consumed per replicate. This is an overestimation, as it is known that the not all of the 20 µL effluent into the LIBS plasma is being excited and/or ionized.

Aerosol LIBS										
Emission Line	Conc (ppm)	SNR	Bias (%)	Precision (%)	LOD (ppm)	LOD (fg)				
Sr II 421	25	28	-0.9	3.1	1	120				
Mg II 279	25	111	7.1	6.7	0.3	30				
Ba II 493	25	30	1.3	5.0	0.7	170				
Ca II 396	25	62	-2.9	0.5	0.6	70				

Table 18. Figures of Merit for Aerosol LIBS

Analysis of a continuous calibration verification (CCV) standards containing 25 μ g/mL produced bias of as low as 0.9% and 1.3% for the emission lines of Sr II 421.5 nm and Ba II 493.4 nm and 2.9% and 6.7% for Ca II 396.3 nm and Mg II 279.5, respectively.

Using the calculated absolute mass for aerosol LIBS, this translates to a LOD of approximately 120 fg for Sr II 421.55 nm, 170 fg for Ba II 493.41 nm, 70 fg for Ca II 396.3 nm and reaches as low as 30 fg for Mg II 279.80 nm. Table 16 summarizes the figures of merit for aerosol LIBS.

5.4 Microdrop Delivery Instrumentation

Two different inkjet printing systems, JetDrive III and Jetlab 4, purchased from Microfab Technologies, Inc. (Plano, TX) were used to conduct the following experiments.

The JetDrive III was an in-laboratory built system with the necessary printing components purchased through Microfab Technologies, Inc. The components consisted of a printhead, LED strobe light, horizontal viewing optics and a Jetserver controller, see Figure 41. The JetDrive III controller, CT-M2-02 was a stand-alone Windows based control program, that had a built in strobe delay and allowed for manipulations of the bipolar waveform.

The printhead was mounted vertically on a 2 inch optical post, which was mounted on a x-y micrometer stage. The printhead was coupled by a Luer connection to a disposable 2.5 mL syringe which provided the negative pressure. The negative pressure provided by the syringe was controlled by adjusting the height to a level adequate to produce the start of a microdrop. The microdrop was visualized with a strobe LED with a 3000 µs window and horizontal optics equipped with a reticle for calibration and determination of proper microdrop parameters. Drop size was determined by viewing images of the drop from a 90° angle using simple graphing software to determine the number of pixels per square mm of the image. Using the formula for volume of a sphere, the drop volume was calculated.

Plexiglas[®] was used to construct two connecting side walls and an upper covering, enclosing the LIBS collection optics and the microdrop printer.



Figure 41. JetDrive III experimental setup and controller

The second system microdrop system used was the Jetlab 4, see Figure 42a. The Jetlab was an upgraded version of the JetDrive III. It provided an automated x-y-z stage, visualization of both the printhead and the substrate to be printed on, see Figure 42b. This system provided automated pressure control which enhanced the printing stability. The automated stage allowed for patterns to be printed. The updated software was more user-friendly and allowing for the drop images to be calibrated with ease.



Figure 42. Jetlab 4 a) Microdrop System and b) viewing optics on Al stub substrate Both inkjet systems used a MJ-A style drop-on-demand dispensing device (printhead), see Figure 43, with a Luer connection for PTFE tubing. The dispensing

devices are suited for aqueous and solvent-based solutions with an orifice diameter of 60 μ m.



Figure 43. Printhead used for microdrop delivery

The microdrop delivery process is controlled by the drive waveform used for the piezoelectric actuator. Microdrops are produced in both systems by trial and error of the waveform parameters.

5.5 Microdrop Printing for LIBS Analysis

Solid calibration standards can be purchased and LIBS utilizes these standards to determine the relative intensity per concentration of analyte. However, these calibration standards do not allow for absolute mass calibrations or calculations for absolute mass limits of detection. Inkjet printing was utilized through the following experiments to deliver microdrops containing picoliter volumes for LIBS analysis. Knowing the volume of each microdrop permitted for the deposition of known mass quantities of analytes onto the sample surface.

Both configurations on inkjet printing were employed. First, drop-on-demand inkjet printing with the Jetlab 4 instrument was used to deliver known analyte mass quantities for quantification and elemental mapping on aluminum stubs. Inkjet printing allowed for a discrete number of drops, a known absolute mass amount, to be delivered at specified locations.

Continuous mode inkjet printing was employed using the JetDrive III in single microdrop LIBS. A continuous flow of microdrops were produced and timed with the laser pulse for single drop, single laser shot analysis.

5.5.1 Microdrop Quantification on Aluminum Stub

The microdrops were deposited onto an aluminum stub (Ted Pella, CA) that were manufactured for SEM analysis. The optimal printing conditions were determined to be a voltage of $\pm 19/-18$ V, a dwell of 12 μ s, an echo of 35 μ s and the rise and fall times were kept constant at 3 μ s. Dr. Joshi-Kumar aided in the operation of the Jetlab 4.

Preliminary studies were first conducted on the aluminum stub by LIBS to examine the constituents above the LOD within the elemental profile. The metals chosen for deposition were Ba and Sr as these were predetermined by LIBS not to be present in the Al matrix. Multi-element calibration standards were prepared from stock solutions of 1000 ppm and made into a concentration of 250 ppm in 5% nitric acid consisting of Ba and Sr. Studies were conducted with analysis of only the Al stub, followed by stub and solvent and finally with the metal solution on Al stub. The metals were deposited into premade craters which were created using a Cetac LSX 500 laser ablation unit (Omaha, NB) equipped with a 266 nm laser. A spot size of 200 µm and 100 shots created a crater 15 µm deep with a 200 µm diameter, see Figure 44. Figure 44a was produced with a scanning electron microscope, Philips XL 30 (Philips, Eindhoven, The Netherlands). Figure 44b and the 3-D images to follow were generated using a Keyence VHS-600 digital microscope (Atlanta, Ga). The craters provided a sample cell for deposition of the microdrops and allowed visualization to accurately aim the laser to the correct location on the sample surface.



Figure 44. Crater on Al stub pre-LIBS analysis a) 200 μm crater on Al stub for microdrop depositionb) Al stub crater with a depth of 15 μm for microdrop deposition

These craters on the aluminum stub were produced having a smaller diameter (~200 μ m) than that of the laser beam (~215 μ m) to ensure complete analyte removal. The inkjet was then used to deliver precise mass loadings of the heavy metals into the craters. The visualization software allows for the substrate that is printed on to be observed during the inkjet process. This is used to verify that the drops delivered do not overfill the shallow crater.

To ensure quantitative accuracy it must be assumed that all of the deposited mass is being removed. As can be seen from this single shot analysis spectrum, Figure 45, there is a linear relationship between the number of laser shots and the decrease in Sr emission intensity illustrating that the greatest amounts of mass are removed during the first laser pulses.



Figure 45. Linear relationship of Sr mass ablated per laser pulse

This experiment was conducted to conclude the number of shots needed to remove all the mass. After many trials were completed, investigating varying the number of drops with

laser pulses, it was determined that 20 laser pulses was sufficient to remove all the deposited mass.

The 20 laser pulse accumulation acquired during LIBS analysis increases the crater depth from ~15 μ m, previously demonstrated in Figure 44 for microdrop deposition, to ~165 μ m depth after LIBS ablation, see Figure 46.





As a result of ablating predominantly the aluminum stub for the microdrop analysis, the background is dominated by aluminum and other major elemental emission lines (Fe, Si and Cu). Focusing in on the analyte's region of interest, a narrow peak is illustrated, produced from the deposition of 150 pg, see Figure 47.



Figure 47. Al stub spectrum with 150 pg of Sr deposited into crater

The spectrum in Figure 47 illustrates there is no other interference from the aluminum matrix or the solvent. The areas around the crater were also analyzed to verify no solution was spilled. The analysis of the area around the crater produced no signal for the analytes of interest.

Varying the number of drops printed in each crater varied the quantity of mass deposited. Calibration curves were produced correlating the absolute mass ablated to the LIBS background subtracted intensity. The number of microdrops printed in each crater varied from 0 to 12 drops of 250 ppm Ba and Sr solution. All points on the calibration curves, see Figure 48, represent an average of 5 replicates and the error bars represent ± 1 standard deviation.



Figure 48. Calibration curves for microdrop LIBS on aluminum stub for a) Sr II 407.7 nm and b) Ba II 614.2 nm

The precision for Ba II 614.2 nm ranged from ~12% RSD for 10 drops (215 pg) to ~20% RSD for 1 drop (21 pg). The precision for Sr II 407.7 nm ranged from ~5% RSD for 6 drops (445 pg) to ~14% RSD for 1 drop (74 pg).

Continuing calibration verification standards (CCV) containing 250 ppm Sr was analyzed to test the bias of this method. For 6 drops (445 pg) a bias was produced of 7.5% corresponding to a 17% RSD and 8 microdrops (594 pg) produced a 6.9% bias and a precision of 7% RSD for Sr. The limit of detection is defined as the smallest measure that can be detected with reasonable certainty for a given analytical procedure and equivalent to $3\sigma + \bar{x}$ where σ is the standard deviation from a range in the background close the signal and \bar{x} is the mean of the background. The calculated LOD for Sr II 407.7 nm and Ba II 614.7nm were ~ 2 pg.

Utilizing inkjet printing for the deposition of metal solutions on aluminum stubs proved to be a viable method for the determination for absolute mass detected with LIBS. The only drawback was the background was dominated by the matrix of the aluminum stub.

5.5.2 Microdrop Mapping with LIBS

LIBS provides rapid elemental analysis and with only removing nanograms to micrograms of mass. LIBS is suited to elementally characterize surfaces with little-to-no sample preparation. Surface mapping by LIBS was reported in the mid 1990's. Hakkanen *et al.* reported good correlation between Ca and Si concentrations in paper¹⁸³. Laserna *et al.* investigated two dimensional mapping of carbon impurities and reported depth resolution of 40 nm¹⁸⁴. Menut *et al.* used LIBS to map the minor constituents of the surface on steel¹⁸⁵. However, Menut *et al.* reported that there was insufficient LIBS signal for trace elements that were measured at the 1% abundance level.

The goal of this next study is to demonstrate that LIBS is a sensitive technique that is capable of characterizing nanogram metal depositions on an aluminum substrate. The Jetlab 4 was programmed by Dr. Joshi-Kumar to print a pattern, see Figure 49.



Figure 49. Jetlab 4 pattern printed for LIBS elemental mapping analysis The software provided with the Jetlab 4 allows for a certain number of microdrops to be dropped at certain predetermined distances from each other. The software was programmed to print the FIU logo with microdrops being spaced 0.25 mm.

Previously, premade craters were utilized for sample deposition and laser focus. This study printed one drop of 5000 ppm Sr solution, in the FIU pattern shown above, on an unaltered aluminum stub shown in Figure 50.



Figure 50. a) aluminum stub with printed pattern, b) aluminum stub after LIBS elemental mapping analysis

The resolution of the LIBS mapping was dependent on laser spot size and smallest distance the x-y stage could translate. A 266 nm laser with a spot size of 215 μ m moved in steps of 200 μ m across the aluminum stub, see Figure 50b. The area elementally mapped by LIBS was ~2.0 cm by 1.2 cm, corresponding to approximately 50 laser craters by 30 laser craters. The line scan was stopped when analytical signal for Sr was blank for

5 replicates. The data for the background subtracted peaks were entered into a Wolfram Mathematica® algorithm written by a previous post-doctoral student, Dr. Barnett, for image mapping. Figure 51 clearly illustrates the FIU logo in a two-dimensional plot.



Figure 51. Two-dimensional plot of LIBS elemental mapping of Sr

A three-dimensional elemental map was also constructed to illustrate the Sr concentration gradient across the aluminum stub, see Figure 52. The printed area relates to the presence of Sr concentration which was spatially mapped by signal intensity. The absolute mass detected for the elemental mapping of Sr was 26 ng seen in the light regions of the plot.



Figure 52. Three-dimensional plot illustrating Sr concentration with LIBS elemental mapping

LIBS has demonstrated to be capable of providing special distribution of elements at very low mass loadings. LIBS could be an alternative method for the mapping of mineral, biological and forensic matrices.

5.5.2 Microdrop Analysis with LIBS in Air

As previously mentioned, the major disadvantage for microdrop LIBS analysis on the aluminum stub was the production of the high background produced as a result ablating predominantly the aluminum stub. In order to remove background inferences, the microdrop need to be analyzed without deposition on any surface.

For this study the JetDrive[™] III controller (Microfab Technologies, Inc., Plano, TX, USA) with a piezo-actuated 60 µm orifice diameter printhead device was used to deliver microdrops of known mass quantities.

The microdrop printing parameters were optimized for drop size, velocity, and reproducibility. The driving waveform bipolar pulse amplitudes were \pm 16 V, a rise and fall time of 3 µs and a dwell time of 20 µs, with an ejection frequency of 250 Hz. All experiments were performed under ambient temperature and pressure. These microdrops of known mass quantities were used to determine the LOD for absolute mass detection, bias and precision of LIBS.

A 532 nm laser was used for microdrop atomization and ionization. LIBS optical emissions were collected and imaged at a 90 degree angle from the plasma. The light was transferred into an AndorMechelle 5000 spectrometer. The experimental setup is seen in Figure 53 below. Five replicates were analyzed and averaged for the calculations.



Figure 53. Experimental LIBS setup for microdrop LIBS in air

To prevent external influences from shifting the microdrop in flight, a Plexiglas shelter was constructed enclosing the collection optics and the microdrop printer. The printhead was placed approximately 4 mm above the formation of the LIBS plasma to reduce the time and length the drop needed to fall.

The drops were spatially and temporally aligned with the LIBS plasma using a PI-MAX nanosecond gated camera. A strobed LED was used for observing droplets in flight to verify that only one drop per LIBS plasma was analyzed. The strobe provided a 3000 µs window, which allowed for visualization before the microdrop had formed, during microdrop formation and flight into the LIBS plasma.

The microdrop images were taken throughout the experiment to determine a drop volume of 90 pL \pm 12 pL. An image of the printhead with a microdrop exiting and a microdrop in the LIBS plasma is shown in Figure 54. The drop size was determined by viewing images of the drop from a 90° angle using simple graphing software to determine the number of pixels per square mm of the image. Using the formula for

volume of a sphere, the drop volume was calculated. With the microdrop having a density of 1 g/cm³, the terminal velocity is calculated to be \sim 75 mm/sec.



Figure 54. A) 90 pL drop ejected from the orifice of the printhead; B) The microdrop in the LIBS plasma being atomized and ionized.

5.5.3 Microdrop Data Analysis

For single drop microdrop LIBS elemental solutions containing Ba, Sr, Mg and Al and were prepared to a final concentration of 0, 10, 15,25, 50, 100, 250, 500, 1000, and 3000 ppm thereby giving an absolute mass of 0, 0.9, 1.4, 2.3, 4.5, 9.0, 22.5, 45.0, 90.0, and 270 pg per drop, respectively. Continuing calibration verification standards (CCVs) were prepared independently and used for method validation and to quantify bias at 25 ppm for 250 ppm (22.5 pg) for single drop microdrop LIBS. The CCVs were analyzed randomly throughout the experimental procedure.

As a result of continuous mode microdrop printing, more microdrops were produced than atomized and ionized by the LIBS plasma. To account for this, a kinetic series of 100 single laser pulses were performed and those with no signal were discarded, \sim 30% of spectra were kept for analysis. Background subtracted peak intensities of the selected emission lines, determined to be free of spectral interferences were used for analysis

5.5.4 Single-Pulse and Double-Pulse Microdrop LIBS

Single-pulse and collinear double-pulse comparisons were conducted for microdrop LIBS at the optimized parameters listed above. As expected, an increase from single to doublepulse was observed. Figure 55 compares the LIBS spectra for single and double-pulse. There is an approximate four-fold increase from single to double-pulse microdrop LIBS.



Figure 55. LIBS spectra of a microdrop double-pulse and single-pulse spectra for Sr peaks 407.7 nm, 421.5 nm and 460.7 nm with 90 picogram of Sr

The signal-to-noise ratio for the Sr II 407.7 nm emission line increased from 10 to 39 and Sr II 421.5 nm emission line signal-to-noise ratio increased from 50 to 212. The signal

enhancement for the atomic Sr 460.7 nm emission line was less at approximately 3 times with a single-pulse signal-to-noise of 25 and a collinear double-pulse of 73.

Single-drops produced volumes of ~90 pL \pm 12 pL and directed to the space where a LIBS plasma would be formed. The varying concentrations of known mass where then jetted into the LIBS plasma and calibration curves were constructed. Weighted regression lines were used to treat the data for the microdrop LIBS as data heteroscedasticity was observed. Using weighted calibration curves allowed for additional weight to be added to the data points where the error was the smallest, thereby allowing for the best fit line to pass closer to those points with small error than to the points with larger error and concentration.38 The LIBS signal response to a known mass concentration was established producing R²>0.99 for both single and double-pulse configurations.

To assess the figures of merit for the single microdrop technique a CCV at a concentration of 250 ppm was used, thereby producing a drop of containing 22.5 pg of the analyte of interest. The precision of the microdrop LIBS was not as good as with aerosol LIBS with values ranging from13% RSD, 16% RSD and 22% RSD for Al II 394.4 nm, Sr II 421.5 nm and Ba II 493.41 nm, respectively. However, single microdrop LIBS was able to achieve a bias of 1% and 5% for emission lines Al II 394.4 nm and Ba II 493.4 nm, and these results are summarized in Table 17.

Microdrop LIBS										
Emission Line	Mass (pg)	Volume (pL)	SNR	Bias (%)	Precision (%)	LOD (pg)				
Sr II 421	45	90	69	2.6	8.3	1				
Mg II 279	45	90	13	9.0	15.2	1				
Ba II 493	45	90	34	-5.1	22.1	1				
Al II 394	45	90	15	1.1	13.2	3				

Table 19. Figures of Merit for Microdrop LIBS in Air

Microdrop LIBS resulted in LODs of approximately 1 pg for Ba II 493.4 nm, Sr II 421.5 nm and Mg II 279.8 nm. The Al II 394.4 nm emission line resulted in a LOD of approximately 3 pg. The larger LOD is the result of the incorporation of the entire drop volume (90 pL) for the observation. Other LIBS researchers such as, Feng *et al.*, found the Pb I 405.7 emission line LOD to be 60 μ g/mL when using a liquid jet at a flow rate of 20 ml/min⁵⁴, Kumar *et al.* used liquid jets at different flows rates, 17.5 ml/min and 3.5 ml/min, and found Mg II 279.8 LOD to be 0.06 μ g/mL⁵³and Knoch *et al.* list a LOD of Mn at 80 μ g/L when forming a cavitation bubble inside the cuvette⁵⁶. Both methods described in this paper use magnitudes of volume less and produce LODs of ~1 μ g/mL (100 fg) for aerosol LIBS and ~1 pg for single drop microdrop LIBS.

5.6 Internal Standardization for Solution Analysis by LIBS

Internal standardization was evaluated for improving sensitivity, precision and bias for both aerosol and microdrop LIBS. Previous research by Ko¹⁸⁶ on solid matrices recommends two conditions should be met for an element to be used as an internal standard: the emission lines need to be close in the broadband spectrum and the excitation of the upper energy levels of the two transitions should be within the same range. During the study different elements and different elemental emission lines of the same element with varying excitation energies were evaluated. Fichet *et al.* previously reported the use of an internal standard as deteriorating the linearity and limit of detection¹⁸⁷, however, Koch *et al.* find internal standardization to improve the signal⁵⁶. During the present study scandium, sodium and copper were used as internal standards and added to have total concentrations in the solutions of 25, 50 or 75 ppm. Off these three different concentrations in aerosol LIBS, 25 ppm scandium produced most favorably with a precision average of 3.4% RSD, a bias of 1% and a LOD of 0.8 ppm. Similar to worse results were obtained for different emission lines and different elements. None of the elements or corresponding emission lines chosen for internal standards elements exhibited a significant improvement for the figures of merit in either aerosol or microdrop LIBS.

5.7 Conclusions

Aerosol LIBS and single drop microdrop LIBS allow for solution samples to be analyzed directly in air or without a carrier gas. These two techniques eliminate certain disadvantages observed with liquid analyses, such as splashing, while also eliminating the greater volume requirements needed for solution sampling by techniques such as ICP-MS or ICP-OES.

When comparing the aerosol to the microdrop LIBS, the microdrop provides the mass in an area confined by the ~ 90 pL microdrop, where the mass ejected and detected in the aerosol is not as confined, thereby the amount of mass detected per unit area is less. Aerosol LIBS is dependent on the accumulation of 20 laser pulses to aid in achieving the low limits of detection. Microdrop LIBS did not use any accumulations, and only one laser pulse was necessary to integrate a 90 pL microdrop.

Data analyzed in both the single and double-pulse configurations resulted in correlation coefficients >0.99 for both methods of aerosol LIBS and single drop microdrop LIBS. Microdrop LIBS on an aluminum stub produced correlation coefficients of ≤ 0.99 .

Quantitative analyses by aerosol LIBS demonstrated an ultra-low limit of detection of ~100 fg for an analytical volume of 20 μ L and produced a precision and accuracy values ranging from as low as 0.5% RSD and 0.9%, respectively in the collinear double-pulse LIBS configuration. Microdrop LIBS is demonstrated to have ultra-low absolute limits of detection of approximately 1 pg in a total analytical volume of 90 pL with an average precision of 14% RSD and an average bias of 4.5%. Microdrop LIBS on an aluminum stub performed similar to single microdrop LIBS producing a low

absolute limit of detection of approximately 2 pg, with an average precision of 12% RSD and an average bias of 8%.

This research demonstrates that LIBS is able to accurately and precisely analyze small volumes of solution \leq 300 µL for aerosol analysis and 90 pL for single-microdrops. These two methods dramatically reduce the total volume needed for analysis when compared to traditional solution sampling methods.

LIBS has shown the capability to accurately map surfaces by their elemental profile. LIBS detected absolute mass amounts less than or equal to 29 ng on the sample surface. The elemental mapping by LIBS was time-consuming; however, elemental mapping done by SED and XRF can take hours also. The advantage to using LIBS is the low limit of detection. LIBS has the potential to provide surface analysis mapping, depth profiling and elemental profiling with high sensitivity.

6.0 Research Conclusions

There have been many significant contributions to the LIBS literature since the first reporting of the use of a laser induced plasma as an excitation source in atomic spectroscopy in 1963⁷⁵. Throughout this research, LIBS has demonstrated to be capable of both a qualitative and quantitative analysis for solutions and solids. One of the main advantage of LIBS is its simplicity. LIBS uses a high-power laser to produce a spark on the sample surface. This results in a high temperature plasma, where the emitted photons are collected from atoms and ions. The evolution of the transient plasma requires temporal gating to obtain the highest analytical signal. The collection of the emitted light allows for identification and quantification of the elements present in the sample. LIBS offers advantages over conventional elemental analysis techniques, in that it provides real time analysis on most all sample matrices without any sample preparation.

Precision is the key in forensic science as a result of comparisons being made between known and questioned samples. The forensic analyst needs to state with a high degree of certainty that the questioned sample is or is not significantly different than the known sample. These comparisons establish whether a sample has originated from a known source or that it is different and the observed differences are greater than the experimental error and sample heterogeneity, combined. LA-ICP-MS is a very sensitive analytical technique that most forensic laboratories in the United States do not have access to because the cost of acquisition and operation is out-of-reach. LIBS is not as sensitive as the competing technique of LA-ICP-MS, however, it has gained interest in that it is able to produce similar results at a fraction of the complexity and cost making it

a very attractive analytical technique for the association and discrimination of glass fragments in the forensic laboratory.

The first study conducted was the optimum laser wavelength for the forensic analysis of glass using LIBS. It was proven that the UV laser provide better lasermaterial coupling and less plasma shielding. This leads to an increase mass amount ablated and an increase in analytical signal. The 266 nm wavelength provided a linear relationship to mass ablated achieving correlation coefficients of >0.990, a precision of ~4.5% RSD for elements ranging from 32-4600 ppm, and LOD where more than adequate to glass analysis. Where the 1064 nm laser still provided analytical data, it destroyed the sample and the precision increased to ~10% RSD.

LIBS was used as an analytical technique for the forensic association and discrimination of glass produced at the same manufacturing plant using the developed method. Two different sample sets were used to assess the discrimination power of an optimized analytical LIBS method for the elemental analysis of glass. The precision of developed method for calculating the ratios was determined to be ~5.5% RSD. The samples ranged in manufacturing date from days to years apart. When all the ratios are combined in a comparison, 99% of the possible pairs were discriminated using the optimized LIBS method. These results support the hypothesis that the elemental composition of glass produced in a single plant over time varies more than the differences that can be detected using analytical LIBS. The round robin studies were evidence that LIBS is able to produce similar results when the method is optimized.

LIBS demonstrates to be a powerful and sensitive technique for the forensic association and discrimination of float glass. LIBS has also shown to provide information

of discrimination on other forensic matrices, such as, drugs¹⁸⁸, explosives^{189,190}, soil¹¹⁵, ink¹⁹¹, cotton²⁷ and paint^{192,193}. LIBS instrumentation is currently being manufactured commercially, allowing LIBS to be easily implemented into forensic laboratories in the future. The portability of LIBS allows for instrumentation to be taken to the crime scene, thereby reducing possible contamination sources. LIBS is an attractive analytical method for forensic laboratories because of the low LODs achieved and the cost of acquisition, operation and maintenance being less than then the well-established techniques.

Finally LIBS was shown capable of low volume (90 pL) quantitative elemental analysis of picogram amounts of dissolved metals in solutions. Single-pulse and collinear double-pulse LIBS were investigated using a 532 nm dual head laser.

The calibration curves produced correlation coefficients with R^2 values >0.99 for both systems. The precision, accuracy and limit of detection (LOD) determined for aerosol LIBS were averaged and determined for the emission lines of Sr II (421.5 nm), Mg II (279.8 nm), Ba II (493.4 nm) and Ca II (396.8 nm) to be ~ 3.8% RSD, 3.1% bias, 0.7µg/mL, respectively. A microdrop dispenser was used to deliver single drops onto an aluminum stub and into air. The microdrops allow for known mass amounts to be deposited onto a sample surface or captured in air.

In the single drop microdrop LIBS experiment, the analysis of a single drop, containing a total mass of 45 pg resulted in a precision of 13% RSD and a bias of 1% for the Al I (394.4 nm) emission line. The absolute limits of detection for microdrop LIBS for the Sr II 421.5 nm emission line was approximately 1 pg for both microdrops on an aluminum stub and in air. Overall, the precision, accuracy and absolute LOD determined for microdrop LIBS resulted in a typical performance of ~ 14% RSD, 6% bias, and 1 pg for the elements Sr II (421.5 nm), Al I(394.4 nm), Mg II (279.8) and Ba II (493.4 nm).

Aerosol LIBS used ~20 μ L per analysis and was able to produce bias of as low as 0.9% for Sr II 421.5 nm the emission line. The LOD of approximately 120 fg was achieved for Sr II 421.5 nm, 170 fg for Ba II 493.4 nm, 70 fg for Ca II 396.3 nm and reached as low as 30 fg for Mg II 279.80 nm.

The real-time analyses of microdrops, aerosols and particles have a wide range of applications. The future of this analytical method is predicted to be implemented for analysis of combustion process monitoring, pollutants of heavy metals in air, waste monitoring into water streams, and atmospheric sciences. The LIBS instrumentation can be manufactured compact and portable which allows for in-situ monitoring of these many applications.

The development and implementation of technical standards is important for the future growth of LIBS as an analytical technique. Standard operating procedures and standard methodology needs to be developed, similar to LA-ICP-MS. The results presented throughout this research demonstrate that LIBS is capable for the analysis of glass as it provides similar discrimination as LA-ICP-MS. LIBS also was proven capable for the analysis of small volumes, thereby competing with the solution technique of ICP-OES.

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Graduate Student Association Scholarly Forum: Oral presentation, February 27, 2012, Florida International University, Miami, FL	

Lawrence Berkeley National Laboratory: Invited seminar speaker, February 1, 2012, Berkeley, CA

The Federation of Analytical Chemistry and Spectroscopy (FACSS): Invited speaker, presentation titled, October 2-7, 2011, Reno, NV

National Institute of Justice 2011 Trace Evidence Symposium: Science, Significance and Impact: Poster presentation, August 8-11, 2011, Kansas City, MO

North American Symposium on Laser Induced Breakdown Spectroscopy (NASLIBS) 2011: Oral presentation, July 18-20, 2011, Clearwater Beach, FL

Graduate Student Association Scholarly Forum: Oral presentation, March 31, 2011, Florida International University, Miami, FL

The Pittsburgh Conference on Analytical Chemistry and Applied Spectroscopy (PITTCON) Meeting 2011: Oral presentation, March 13-18, 2011, Atlanta, GA

NIJ Sponsored Elemental Analysis Working Group Meeting 2010: Oral presentation, December 1-3, 2010, Florida International University, Miami, FL

6th International Conference of Laser-Induced Breakdown Spectroscopy 2010: Poster presentation, September 13-17, 2010, Memphis, TN

NIJ Sponsored Elemental Analysis Working Group Meeting 2010: Oral presentation, Aug. 13, 2010, Breckenridge, CO

American Chemical Society FAME (Florida Annual Meeting and Exposition) 2010: Oral presentation, May 13-15, 2010, Palm Harbor, FL

Graduate Student Association Scholarly Forum: Oral presentation, March 22, 2010, Florida International University, Miami, FL

American Academy of Forensic Sciences 2010: Oral presentation, February, Seattle, WA

North American Symposium on Laser Induced Breakdown Spectroscopy (NASLIBS) 2009: Poster presentation, July 13-15, 2009, New Orleans, LA

American Chemical Society FAME (Florida Annual Meeting and Exposition) 2009: Oral presentation, Orlando, FL

American Academy of Forensic Sciences 2008: Poster presentation, February, San Antonio, TX