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Wei Song

*Northwestern University; Harbin Institute of Technology*

Qing Wei

*Northwestern University*

Wenzhong Liu

*Northwestern University*

Tan Liu

*Northwestern University*

Ji Yi

*Northwestern University*

*See next page for additional authors*

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**Authors**

Wei Song, Qing Wei, Wenzhong Liu, Tan Liu, Ji Yi, Nader Sheibani, Amani A. Fawzi, Robert A. Linsenmeier, Shuliang Jiao, and Hao F. Zhang



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H.F.Z. (hfzhang@  
northwestern.edu)\* These authors  
contributed equally to  
this work.

# A combined method to quantify the retinal metabolic rate of oxygen using photoacoustic ophthalmoscopy and optical coherence tomography

Wei Song<sup>1,6\*</sup>, Qing Wei<sup>1\*</sup>, Wenzhong Liu<sup>1\*</sup>, Tan Liu<sup>1</sup>, Ji Yi<sup>1</sup>, Nader Sheibani<sup>2</sup>, Amani A. Fawzi<sup>3</sup>, Robert A. Linsenmeier<sup>1,3,4</sup>, Shuliang Jiao<sup>5</sup> & Hao F. Zhang<sup>1,3</sup>

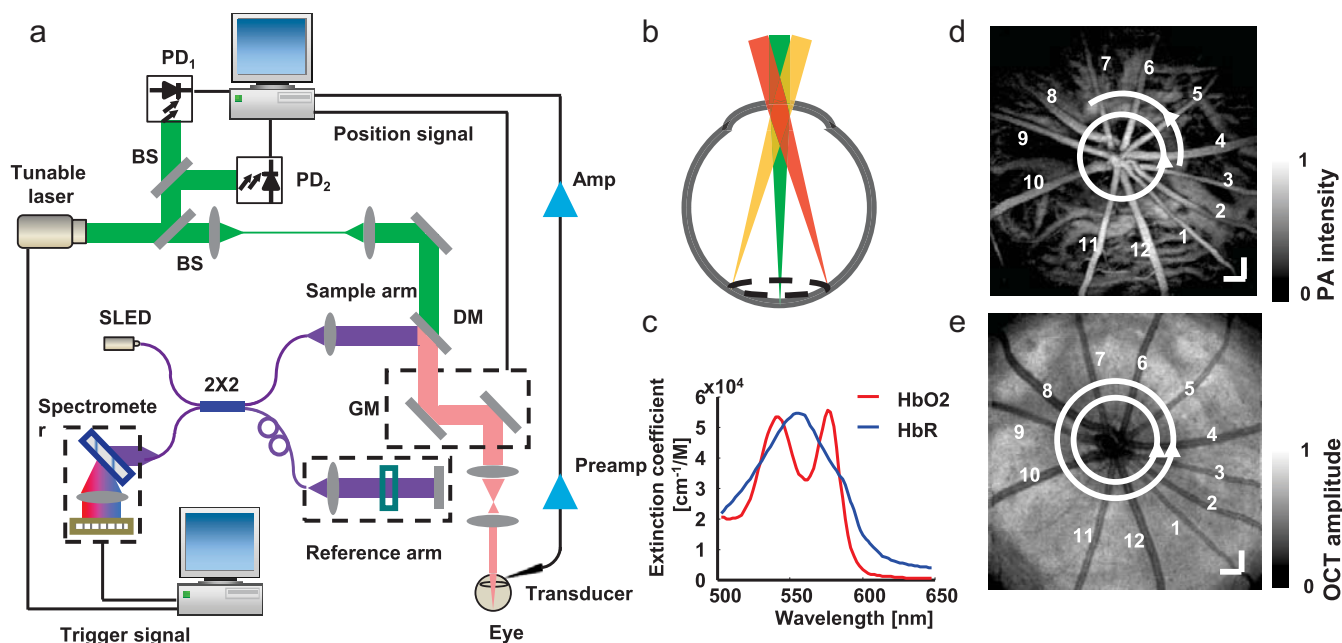
<sup>1</sup>Department of Biomedical Engineering, Northwestern University, Evanston, IL 60208, USA, <sup>2</sup>Department of Ophthalmology and Visual Sciences, University of Wisconsin-Madison, WI 53792, USA, <sup>3</sup>Department of Ophthalmology, Northwestern University, Chicago, IL 60611, USA, <sup>4</sup>Department of Neurobiology and Physiology, Northwestern University, Evanston, IL 60208, USA, <sup>5</sup>Department of Biomedical Engineering, Florida International University, Miami, FL 33174, USA, <sup>6</sup>Department of Physics, Harbin Institute of Technology, 92 West Da-Zhi Street Nangang District, Harbin, Heilongjiang 150080, China.

**Quantitatively determining physiological parameters at a microscopic level in the retina furthers the understanding of the molecular pathways of blinding diseases, such as diabetic retinopathy and glaucoma. An essential parameter, which has yet to be quantified noninvasively, is the retinal oxygen metabolic rate (rMRO<sub>2</sub>). Quantifying rMRO<sub>2</sub> is challenging because two parameters, the blood flow rate and hemoglobin oxygen saturation (sO<sub>2</sub>), must be measured together. We combined photoacoustic ophthalmoscopy (PAOM) with spectral domain-optical coherence tomography (SD-OCT) to tackle this challenge, in which PAOM measured the sO<sub>2</sub> and SD-OCT mapped the blood flow rate. We tested the integrated system on normal wild-type rats, in which the measured rMRO<sub>2</sub> was 297.86 ± 70.23 nl/minute. This quantitative method may shed new light on both fundamental research and clinical care in ophthalmology in the future.**

The demand for treating blindness and low vision continue to escalate as human longevity increases worldwide. By 2004<sup>1</sup>, for example, blindness and low vision had affected more than three million Americans aged 40 years and older; by 2010<sup>2</sup>, 285 million people globally were affected. More than 80% of such visual impairments were caused by eye diseases<sup>1</sup>, which include glaucoma, diabetic retinopathy (DR), age-related macular degeneration (AMD), and cataracts<sup>1,2</sup>. Alterations in oxygen metabolism are believed to be involved in most of these diseases<sup>3,4</sup>. For instance, hypoxia in the glaucomatous retina can damage the optic nerve head, partially due to insufficient vascular perfusion<sup>5</sup>. In DR, the loss of pericytes is often associated with poorly regulated blood flow<sup>6</sup>, which can further lead to retinal vascular occlusion and retinal hypoxia<sup>7</sup>. In AMD, abnormalities in retinal perfusion have also been reported<sup>8</sup>. Perturbations in retinal oxygenation can prompt, for example, degeneration of retinal neurons, loss of photoreceptors, and onset of neovascularization, eventually causing visual impairment. Therefore, the precise measurement of retinal oxygen metabolic rate (rMRO<sub>2</sub>) can be critical in investigating these blinding diseases.

Non-invasive rMRO<sub>2</sub> quantification has been proposed for decades<sup>9,10</sup> without being successfully demonstrated. Obtaining rMRO<sub>2</sub> measurements is challenging because it requires measuring retinal blood flow and oxygen saturation (sO<sub>2</sub>) together. Advances in Doppler spectral domain optical coherence tomography (SD-OCT) makes it possible to precisely detect retinal blood flow<sup>11</sup>. The main obstacle is accurately measuring retinal sO<sub>2</sub>. To measure retinal sO<sub>2</sub>, researchers have used oxygen-sensitive electrodes and magnetic resonance imaging<sup>12–15</sup>, but these efforts are usually restricted to terminal experiments and/or limited by low spatial resolution.

To resolve retinal sO<sub>2</sub> noninvasively and with a high spatial resolution, researchers have mainly focused on multi-spectral fundus photography based oximetry<sup>16</sup>. Owing to the distinct light absorption spectrum between oxygenated and deoxygenated hemoglobins<sup>16,17</sup>, multi-wavelength fundus photography can assess the sO<sub>2</sub> in retinal vessels. Specifically, optical density of a retinal blood vessel, which is the logarithm of the ratio between detected backscattered light intensities from the vessel and its adjacent retinal tissues<sup>16</sup>, is obtained at several



**Figure 1 | Illustration of integrated PAOM and SD-OCT to measure rMRO<sub>2</sub>.** (a) Schematic of the experimental setup. (b) Circular scanning pattern on the retina. (c) Molar extinction coefficient spectrum of oxy- and deoxy-hemoglobin. (d) A maximum-amplitude-projection PAOM fundus image showing 12 major retinal vessels. The circle (radius: 0.45 mm) and the concentric arc (radius: 0.56 mm) are scanning trajectories from which PAOM B-scan images were acquired for assessing sO<sub>2</sub>. Bar: 200 μm. (e) An OCT fundus image of the same rat showed in the panel d. The circles (radii of 0.45 and 0.56 mm) highlight the scanning trajectories for measuring Doppler angle and blood flow. Bar: 200 μm.

selected illumination wavelengths. Hickham *et al.* first applied two-wavelength fundus photography to map retinal sO<sub>2</sub><sup>18</sup>, yet two-wavelength fundus photography is sensitive to light scattering and is easily affected by retinal local parameters such as vessel size, melanin concentration in retinal pigment epithelium<sup>16</sup>. To improve the stability and accuracy in sO<sub>2</sub> measurement, researchers employed additional wavelengths in fundus photography in later studies to compensate for the effect of optical scattering, as well as the vessel size<sup>19–22</sup>. In addition, researchers chose wavelengths 548 nm and 610 nm to correct the influence of melanin based on the approximate linearly decreased extinction coefficient of melanin within this wavelength range<sup>23</sup>. Building on such modifications, the performance of retinal oximetry was much improved. However, adding more wavelengths cannot completely eliminate the influence from optical scattering and variations of retinal local parameters<sup>16</sup>. Our recent numerical simulation study demonstrated that the absolute measured sO<sub>2</sub> error could be up to be 20% when the vessel size is as large as 160 μm or the melanin concentration in the retinal pigment epithelium is as high as 8 mmol/L<sup>24</sup>.

Optical coherence tomography (OCT) has the potential to measure retinal sO<sub>2</sub> measurement<sup>25,26</sup> noninvasively. We recently explored the feasibility of using visible-light OCT (Vis-OCT) to quantify retinal sO<sub>2</sub> *in vivo*<sup>27</sup>; yet there is still a long way before OCT can be verified to precisely measure sO<sub>2</sub> at various anatomical sites. The capability of photoacoustic (PA) imaging to quantify sO<sub>2</sub>, however, has been well-studied and well-documented in various anatomical sites, including the ears<sup>28</sup>, esophagus, colon<sup>29</sup>, and brain<sup>30</sup>.

Building on the proven strength of PA imaging<sup>31</sup>, we developed photoacoustic ophthalmoscopy (PAOM) to address the aforementioned need in retinal metabolic imaging using rats as an animal model. We further optimized a multi-wavelength methodology in PAOM to quantify retinal sO<sub>2</sub>.

## Results

**Imaging schematic for both sO<sub>2</sub> and flow quantification.** We accessed rMRO<sub>2</sub> by integrating PAOM with Doppler SD-OCT.

Figure 1a illustrates the combined functional imaging system (see Online Methods for more details.). The aligned and collimated probing beams for both PAOM and SD-OCT were scanned by the same optics on the retina for imaging. We employed a circular scanning pattern centered at the optic disc to image all the retinal vessels within single B-scans as shown in Figure 1b. The molar extinction coefficients of oxy-hemoglobin (HbO<sub>2</sub>) and deoxy-hemoglobin (HbR) can be found in Figure 1c, based on which sO<sub>2</sub> can be measured by multi-wavelength PAOM. The accuracy of PAOM was validated by measuring a series of *ex vivo* bovine blood (Quad Five Inc, Ryegate, MO) phantom samples with different preset sO<sub>2</sub> levels (see Supplementary Figure S1 and Supplementary Table S1 for more details). A typical anatomical fundus image acquired by PAOM is shown in Figure 1d (see Supplementary Figure S2 for 3D visualization). In Figure 1d, the white circle and arc were scanning trajectories, from where PA signals were extracted for sO<sub>2</sub> measurement. To obtain retinal blood flow, we employed dual-beam scanning in SD-OCT. Corresponding SD-OCT fundus image is shown in Figure 1e; where the two white circles highlight the scanning trajectories used to measure Doppler angle and phase.

**Quantification of retinal sO<sub>2</sub> by multi-wavelength PAOM.** The steps to measure sO<sub>2</sub> using multi-wavelength PAOM are illustrated in Figure 2. We scanned along the highlighted circular trajectory around the optic disk at three wavelengths (570, 578, and 588 nm). Scanning around the optic disk enabled us to measure the complete hemodynamic properties of the eye from a fast one-dimensional scan. The B-scan images along the circular trajectory at the three-wavelengths are shown in the top part of Figure 2a. Fluctuations of the vessels' position along the vertical direction reflect the distances from the vessels to the ultrasonic detection. The PA amplitudes of the 12 major vessels were extracted and are shown below their corresponding B-scan images. We then used the multi-wavelength PA amplitudes of the vessels to estimate sO<sub>2</sub> in every vessel based on the molecular extinction coefficients of HbO<sub>2</sub> and HbR at corresponding optical wavelengths (Figure 1c). The steps to extract



vessel PA amplitude from B-scan images are detailed in Supplementary Figure S3. After inverse calculation, the  $sO_2$  values of all the highlighted vessels scanned along the circular trajectory are given in Figure 2b and Figure 2c. On average, our results show the  $sO_2$  values in arterial and venous blood to be  $93.0 \pm 3.5\%$  and  $77.3 \pm 9.1\%$ , respectively. Shonat et al. pioneered the measuring of retinal oxygen partial pressure ( $PO_2$ ) based on phosphorescence quenching techniques in cats<sup>32</sup>. They reported that the cat's venous  $PO_2$  was 30 Torr, which corresponded to a 42%  $sO_2$  based on the oxygen-hemoglobin dissociation curve in cat<sup>33</sup>. Their measurements were consistent with other reported results in cats<sup>33</sup>. Different animal models are shown to have different retinal oxygenations<sup>34,35</sup>; the rodent's venous  $sO_2$  was reported to be around 70%<sup>36,37</sup>, which agrees with our PAOM measurements.

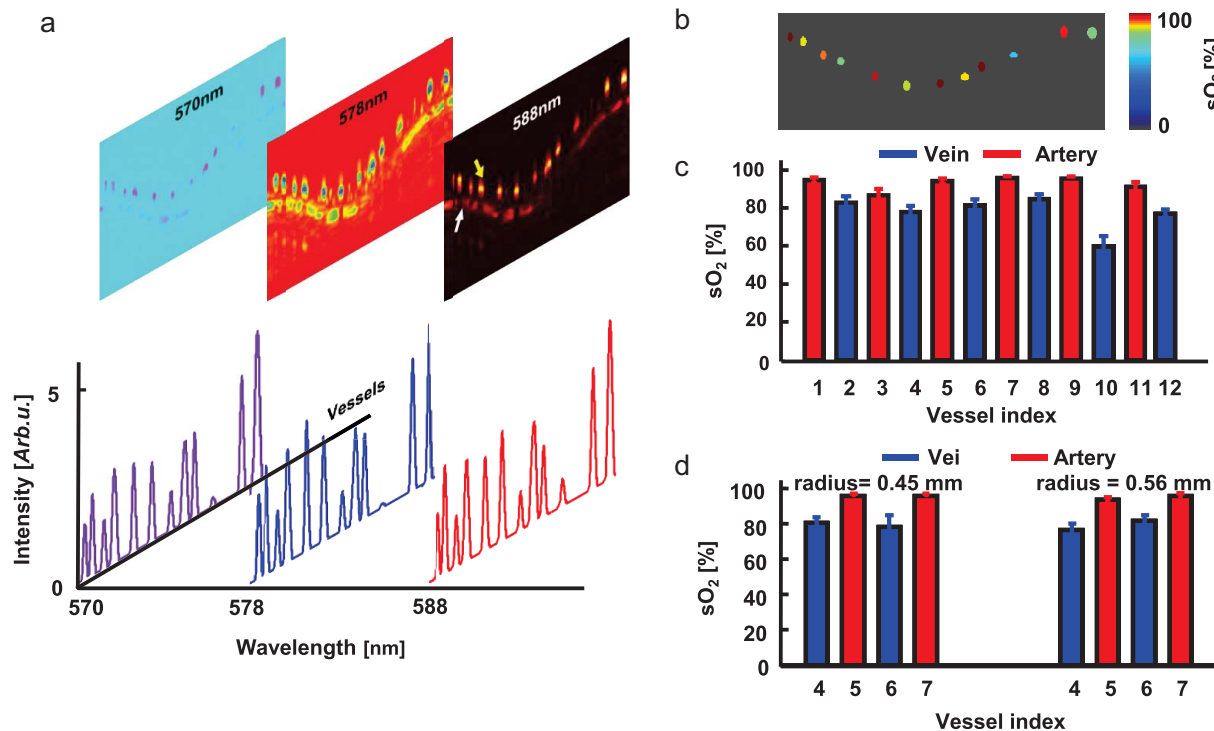
Spatial consistency in  $sO_2$  measurements along the same vessels is essential, but it was not successfully demonstrated in existing retinal oximetry due to influences from retinal vessel diameter and retinal pigmentation variation<sup>16,24</sup>. We tested our spatial consistency by comparing  $sO_2$  measurements from four selected vessels scanned at different positions from the optic disk, as highlighted in Figure 1d. The radii of the two circles were 0.45 mm and 0.56 mm, a separation that is small enough where  $sO_2$  values at the two locations should be the same in each vessel. Results shown in Figure 2d confirm such consistencies, with the largest absolute variation found to be 3.9%.

**Quantification of retinal flow by Doppler SD-OCT.** Figure 3 shows the steps to quantify retinal blood flow velocity and vessel diameter using Doppler SD-OCT<sup>38,39</sup>. Because Doppler SD-OCT can only access the projected blood flow velocity along the probing beam, the Doppler angle (defined as the angle between the vessel and the probing beam) is required to estimate the absolute velocity. We adopted the dual-ring scanning method<sup>38,39</sup> used by several groups

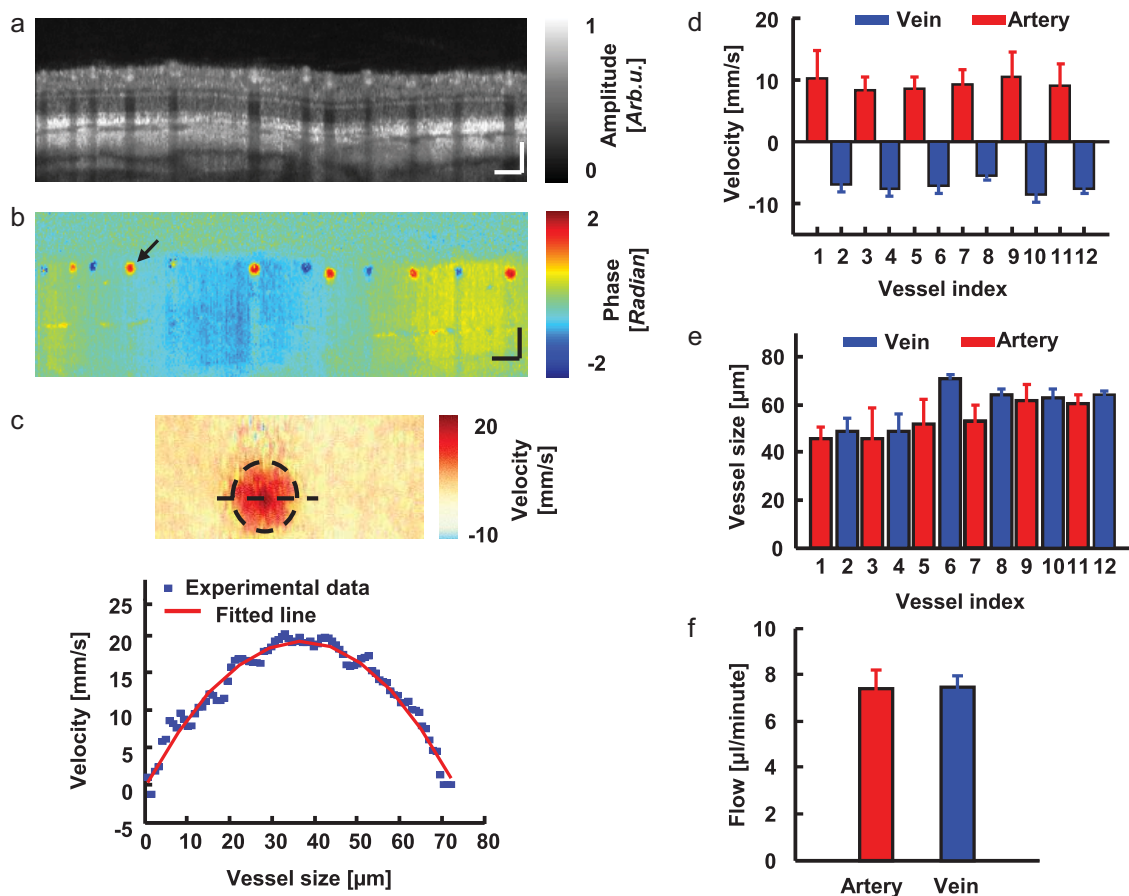
to determine the Doppler angle (see Supplementary Figure S4). The two circular trajectories overlapping with those in PAOM are highlighted in the OCT fundus image (Figure 1e). The OCT B-scan amplitude and phase images (before bulk motion correction) from the inner scanning trajectory are shown in Figure 3a, and Figure 3b, respectively. We obtained the blood flow velocity in each vessel based on the calculated OCT phase variations and their corresponding Doppler angles.

Figure 3c shows a magnified view of the imaged blood flow velocity distribution in a typical vessel (highlighted by the arrow in Figure 3b). The laminar flow profile along the vessel's horizontal centerline clearly shows a quadratic dependence on radii within the vessel. Figure 3d provides the overall measurements of blood flow velocities in this particular retina, from which we can observe higher velocities in arteries than veins. We also extracted the vessel diameter from SD-OCT phase images using a recently developed automatic segmentation algorithm<sup>40</sup>, with results given in Figure 3e. The vessel diameters are shown in Figure 3e, where the veins have larger diameters than the arteries. By multiplying blood velocity with vessel cross-sectional size, we can calculate total retinal blood flow as  $7.43 \pm 0.51 \mu\text{l/minute}$  and  $7.38 \pm 0.78 \mu\text{l/minute}$  within the venous and arterial systems, respectively (Figure 3f). The results are consistent with previously reported results<sup>41</sup> and the venous and arterial blood flows match each other well.

**Quantification of  $rMRO_2$ .** With  $sO_2$  and blood flow acquired, the  $rMRO_2$  can be, therefore, calculated. For the particular retina whose  $sO_2$  and flow we present in Figure 2 and Figure 3, the measured  $rMRO_2$  of the complete inner retina is  $373.41 \pm 88.04 \text{ ng/minute}$ , or  $297.86 \pm 70.23 \text{ nl/minute}$ . This is lower than the 499 nl/minute measured by Shahidi et al<sup>42</sup>. As they pointed out, their  $rMRO_2$  result was higher than other reported values<sup>42</sup>, which was suggested to be caused by measurement variations in some important parameters,



**Figure 2 | Steps to quantify retinal  $sO_2$  using multi-wavelength PAOM.** (a) Cross-sectional retina image acquired at 578 nm, 580 nm, and 588 nm illuminating wavelengths. Top: raw PAOM B-scan images in pseudo-colors. In the 588-nm image, the yellow arrow highlights retinal blood vessels and the white arrow highlights choroidal vessels. Bottom: PA amplitudes of the 12 vessels. (b) pseudo-colored vessels as imaged in the circular PAOM B-scan based on their measured  $sO_2$  values; (c) comparison of  $sO_2$  values in all major vessels. (d) Measured  $sO_2$  in selected vessels from different radii as shown in Figure 1b, where spatial consistency is demonstrated.



**Figure 3 | Steps to measure retinal blood flow using SD-OCT.** (a) OCT B-scan amplitude image acquired from the inner circle as shown in Figure 1c. (b) OCT B-scan phase image from the inner circle. (c) Blood velocity distribution within the vessel highlighted by the black arrow in panel b. Top: two-dimensional distribution along the vessel cross-section; Bottom: experimental and fitted transverse velocity profiles along the horizontal position highlighted by the dashed line. (d) Average blood flow velocity in all the major retinal vessels. The positive velocity of arterial blood shows flow coming from the optic disk to peripheral areas; the negative velocity of venous blood indicates flow coming from peripheral areas to the optic disk. (e) Calculated vessel diameters of all the major retinal vessels. (f) Comparison of the measured total arterial and venous blood flows.

such as the retinal mass. In their results, the venous  $sO_2$  was around 50% (after converting the oxygen partial pressure into  $sO_2$  value based on the dissociation curve), which was lower than the reported normal rodent venous  $sO_2$  value of around 70%<sup>36</sup>. Also, their measured total retinal blood flow in the inner retina was 10.06  $\mu\text{l}/\text{min}$ , which was higher than other reported values<sup>43</sup>. We think that different anesthesia conditions may also contributed to the discrepancy between our and Shahidi's measurements.

## Discussion

Compared with other reported retinal functional imaging modalities, our integrated PAOM and Doppler SD-OCT approach to measure  $rMRO_2$  is advantageous in several aspects. First, our method completely interrogates  $rMRO_2$  noninvasively. Most of the currently reported retinal functional imaging methods<sup>13,16,39,41</sup> can measure only one functional parameter, either retinal  $sO_2$  or blood flow, which is insufficient for  $rMRO_2$  quantification; other proposed imaging modalities that can quantify  $rMRO_2$  are invasive<sup>42</sup>, which is not suitable for *in vivo* applications. Secondly, PAOM is expected to assess retinal  $sO_2$  much more accurately than the multi-wavelength fundus photography<sup>24</sup>.

Our simulation studies suggested that such an improvement originates from the better quantification of blood optical absorption by PAOM than the multi-wavelength fundus photography<sup>24</sup>. Fundus photography estimates light absorption within blood from the collected retinal light reflectance<sup>16</sup>. Several factors deteriorated the accu-

racy of the indirect light absorption measurement. First, the acquired reflected light from the vessel is a superposition of photons, which may have no interaction, partial, or full interaction (travelled through the entire vessel) with the retinal blood. Among these photons, only fully interacted photons can provide accurate measurement of the optical absorption by blood<sup>24</sup>. Secondly, photons backscattered from the vessel's neighboring areas interact more (scattering/absorption) with the melanin in the retinal pigment epithelium (RPE) layer than photons reflected from vessels, because high absorption or scattering by blood allows only a few photons to enter into the RPE. Additional details on how scattering affects fundus photography measurements can be found in our previous Monte Carlo simulation studies<sup>24</sup>.

For multispectral PAOM, the imaging contrast is based on optical absorption from blood or RPE melanin within the visible light spectral range<sup>31</sup>. The absorbed photons can be either ballistic or scattered photons. In the current study, the time-resolved light induced acoustic signals can provide axial resolution of up to 23  $\mu\text{m}$ , which enables us to separate the signals of retinal blood vascular from the RPE melanin given the retina thickness is around 200  $\mu\text{m}$ <sup>44</sup>. As a result, PAOM signals generated from major vessels can be considered to be mainly generated from hemoglobin. Optical scattering, however, does affect the resolution of PAOM. It's reported that the lateral resolution can be degraded by 14% in turbid media compared with the case of no scattering when the imaging depth is close to the transport mean free path<sup>45</sup>. In PAOM, the theoretical lateral resolu-



tion is estimated to be 20  $\mu\text{m}$ . Considering a 14% degradation, the lateral resolution will be reduced to 22.8  $\mu\text{m}$ . Since the degradation in lateral resolution is merely 10% of the theoretical lateral resolution, it may not influence our experimental results much. In addition, the rat eye is notable for its stronger chromatic aberration<sup>46,47</sup>, we analyzed the chromatic aberration effects on the PAOM image within a bandwidth as short as 18 nm, and it turned out the chromatic effects on imaging is small, and should not affect the accuracy of PAOM results (see Supplemental Figure S5 for more details.)

Although versatile and unique, the combined PAOM and SD-OCT imaging system has the following limitations. One major concern comes from ultrasonic signal detection. First, ultrasonic signal detection requires physical contact, as in the experiment, where we coupled a needle ultrasonic transducer to the rodent eyelid with ultrasonic gel<sup>48</sup>. This ultrasonic signal detection scheme is not preferred in clinical settings. Second, the large size and opacity of the needle ultrasonic piezoelectric detector requires a long working distance, which forces a small NA for OCT and thus limits its imaging quality<sup>48</sup>. To overcome this, we recently developed a transparent micro-ring resonator for ultrasonic signals detection, which has a physical dimension of a few millimeters and a much lower noise equivalent pressure<sup>49</sup>. We plan to fabricate this micro-ring resonator onto a contact lens serving as the ultrasonic detector, which requires no ultrasonic gel coupling and allows for a flexible working distance. Thirdly, visual stimulus is reported to increase the retinal vessel diameter and blood flow, as well as affect the retinal  $\text{sO}_2$  through the process of retinal neurovascular coupling<sup>43,50</sup>. These may affect the accuracy of the PAOM. It has been demonstrated that the neurovascular coupling depends on visual stimulus frequency and stimulus duration<sup>51</sup>, where the examined flickering frequency, within our understanding, ranged from 10 to 60 Hz with a typical stimulation time last more than 10 s. Such a condition does not exist in PAOM, where we used 25-kHz A-line rate and 2.5 s total illumination time at each illuminating wavelength. Whether each PAOM illumination will introduce effective neurovascular coupling and lead to an observable hemodynamic response within each acquisition needs further investigation in the future. Lastly, despite the good match between measured  $\text{sO}_2$  by PAOM and the preset  $\text{sO}_2$  in blood phantom experiments (Supplemental Figure S1), we also understand that the phantom experimental conditions are different from those in *in vivo* rodent experiments. For example, there are eye movements during imaging, aberration from the eyeball, etc. Whether such differences will affect the  $\text{sO}_2$  quantification or not also require more future validation.

Another concern is that the performance of dual-ring scanning SD-OCT may be influenced by eye movement due to the consecutive and non-simultaneous scanning sequence of the small and big ring. In our present study, we averaged the vessels' central positions across eight pairs of small-big scanning patterns to prevent motion-induced variation. A motion-insensitive alternative is to scan a pair of small and big rings simultaneously<sup>38</sup>, which further complicates the imaging system. Also, we measured the vessel diameter axially because OCT offers higher axial resolution than lateral resolution, and we calculated the vessel cross-sectional area using the axial diameter by assuming a cylindrical vessel profile as other researchers did<sup>52</sup>.

Dysfunctions in the oxygen metabolic rate ( $\text{MRO}_2$ ) are not merely limited to the retina, as  $\text{MRO}_2$  also has been found to be involved in other diseases, such as cancer<sup>53</sup>, Alzheimer's disease<sup>54</sup>, and heart failure<sup>55</sup>. Owing to its capability to accurately assess  $\text{MRO}_2$ , our multimodal imaging technology can help better understand a wider spectrum of disease mechanisms beyond blinding diseases.

## Methods

**Experimental setup.** A schematic of the experimental setup is shown in Figure 1a. We used a tunable dye laser (Cobra, Sirah Laser and Plasmachnik GmbH) pumped by a pulsed Nd:YLF laser (IS8II-E, Edge-Wave GmbH; pulse duration: 5 ns) as the

illumination source for PAOM. The tunable laser output was collimated into 2 mm in diameter, then merged with the light of SD-OCT (center wavelength: 840 nm; bandwidth: 50 nm; SLED IPSDD0804, InPhenix). A two-dimensional galvanometer scanned the combined light beams (QS-7, Nutfield Technology) and relayed them to the eye through a telescopic lenses system. In PAOM, acoustic waves induced by light absorption were detected by an unfocused small-footprint ultrasonic transducer (central frequency: 40-MHz; bandwidth: 30-MHz; active element size:  $0.5 \times 0.5 \text{ mm}^2$ ) attached to the rat's eyelid through ultrasonic gel. The detected photoacoustic signals were amplified by two amplifiers (ZFL-500LN+, Mini-circuits, and 5073PR, Olympus, total gain: 60 dB) and digitalized by a data acquisition card (CS14200, Gage Applied Technology) at a sampling rate of 200 MS/s. In SD-OCT, backscattered light from the retina first interfered with the reference arm light, then sampled by a home-made spectrometer at an A-line rate of 25-kHz. The lateral resolutions of both PAOM and SD-OCT were around 20  $\mu\text{m}$  in the retina with a slight difference caused by the different spectral ranges. The axial resolutions of PAOM and OCT were 23  $\mu\text{m}$  and 5.6  $\mu\text{m}$ , respectively<sup>56</sup>.

During imaging, a  $256 \times 256$  A-lines scanning pattern was employed to acquire fundus images in both SD-OCT and PAOM. The circular B-scanning (each B-scan contains 4096 A-lines, A-line rate 25-kHz) was used for flow and  $\text{sO}_2$  measurement. In Doppler OCT, we performed eight pairs of big-small circular scans. We confirmed that 25-kHz A-line rate is able to precisely assess retinal blood flow by comparing the measurement at 25-kHz with results acquired by a 70-kHz A-line rate OCT, which is considered sufficiently high to acquire the entire pulsatile flow profile<sup>57</sup> (see Supplementary Figure S6 for more details). In PAOM, the illuminating laser energy was 40 nJ/pulse, which is considered eye-safe as detailed in Supplementary Materials. For  $\text{sO}_2$  detection, at each wavelength, we scanned 16 consecutive circles centered on optical disc with 4096 A-lines in each circle. The time-resolved photoacoustic signals were collected in each A-line. After data collection, we first reconstructed the 16 B-scan images at each wavelength and then sequentially estimated the  $\text{sO}_2$  from the 1<sup>st</sup> B-scan to the 16<sup>th</sup> B-scan. Finally, all the  $\text{sO}_2$  measurements for each vessel were averaged across the 16 B-scan results.

**Animal Preparation.** We used wild-type rats (Sprague Dawley, 300 g, Harlan Laboratories, Indianapolis, IN) in our studies. During experiments, a mixture of isoflurane and normal air was supplied to the rats through a commercial non-rebreathing ventilating system (Vaporizer Inc, Rockmart, GA). We first placed the rat into an induction chamber and adjusted the vaporizer to 2% isoflurane vapor output percentage, setting the attached gas flowmeter at 3 L/min. The vaporizer and flowmeter setting corresponded to 12 mL/hour anesthetic agent gas consumption and were maintained for 10 minutes; then changed to 1.5% isoflurane and 2 L/min air flow for additional five minutes, corresponding to 6.6 mL/hour anesthetic agent gas consumption. At this point, the rat was under deep anesthesia. We then placed the rat on a homemade adjustable holder for imaging. The homemade holder was connected to the ventilation system, which kept the rat ventilated at the rate corresponding to 6.6 mL/hour isoflurane gas consumption. We dilated the rats' pupils with a 1% Tropicamide ophthalmic solution and paralyzed the iris sphincter muscle with a 0.5% Tetracaine hydrochloride ophthalmic solution. Meanwhile, artificial tears (Systane, Alcon Laboratories, Inc.) were applied every other minute to prevent corneal dehydration. During the experiment, the rats' electrocardiogram was monitored (ETH-256 Amplifier, Iworx). Their blood oxygen saturation levels were measured to be around 90% and the heart rate was measured to be around 223 bpm (Pulse oximetry, Model 8500AV, Nonin Medical, Inc).

All experimental procedures were in compliance with ARVO Statement for the Use of Animals in Ophthalmic and Vision Research, and laboratory animal protocol approved by the Institutional Animal Care and Use Committee at Northwestern University.

**$\text{sO}_2$  quantification.** We selected three wavelengths (570, 578, and 588 nm) for  $\text{sO}_2$  imaging in PAOM. The  $\text{sO}_2$  value of each vessel was estimated as follows:

$$\text{sO}_2(x, y, z) = \frac{[\text{HbO}_2]_{(x, y, z)}}{[\text{HbO}_2]_{(x, y, z)} + [\text{HbR}]_{(x, y, z)}}, \quad (1)$$

where [HbR] and [HbO<sub>2</sub>] are the concentrations of oxy- and deoxy-hemoglobin [g/L]. [HbR] and [HbO<sub>2</sub>] were quantified through optical absorption by retinal blood. The blood absorption coefficient can be expressed as

$$\mu_a(\lambda_i) = \varepsilon_{\text{HbR}}(\lambda_i) \cdot [\text{HbR}] + \varepsilon_{\text{HbO}_2}(\lambda_i) \cdot [\text{HbO}_2], \quad (2)$$

where  $\varepsilon_{\text{HbR}}(\lambda_i)$  and  $\varepsilon_{\text{HbO}_2}(\lambda_i)$  are the known molar extinction coefficients [ $\text{cm}^{-1}\text{M}^{-1}$ ] of HbR and HbO<sub>2</sub> at wavelength  $\lambda_i$  [nm], respectively. In PAOM, the detected PA amplitude  $\text{pa}(x, y, z, \lambda_i)$  is considered to be proportional to the local optical energy deposition  $\phi(x, y, z, \lambda_i)$ , which is a product of local  $\mu_a(x, y, z, \lambda_i)$  and local optical fluence  $F(x, y, z, \lambda_i)$ . Thus, Eq. 2 can be rewritten as:

$$\begin{aligned} \text{pa}(\lambda_i, x, y, z) &= K_1 \cdot \phi(\lambda_i, x, y, z) \\ &= K_1 \cdot F(x, y, z, \lambda_i) \cdot (\varepsilon_{\text{HbR}}(\lambda_i) \cdot [\text{HbR}] + \varepsilon_{\text{HbO}_2}(\lambda_i) \cdot [\text{HbO}_2]), \end{aligned} \quad (3)$$

where  $K_1$  is the proportionality coefficient. By assuming consistent optical illumination and ignoring optical attenuation in the retina, we can consider



$F(x, y, z, \lambda_i)$  to be constant and simplify  $K_1 \cdot F(x, y, z, \lambda_i)$  as  $K_2$ . For multiple wavelength PA measurements, Eq. 3 becomes

$$PA = K_2 MH \quad (4)$$

$$\text{where } M = \begin{bmatrix} \varepsilon_{HbR}(\lambda_1) & \varepsilon_{HbO_2}(\lambda_1) \\ \vdots & \vdots \\ \varepsilon_{HbR}(\lambda_n) & \varepsilon_{HbO_2}(\lambda_n) \end{bmatrix}, H = \begin{bmatrix} [HbR] \\ [HbO_2] \end{bmatrix}, \text{ and } PA(x, y, z) = \begin{bmatrix} pa(\lambda_1, x, y, z) \\ \vdots \\ pa(\lambda_n, x, y, z) \end{bmatrix}.$$

Although  $[HbR]$  and  $[HbO_2]$  can only be estimated as relative values, the final  $sO_2$  in Eq. 1 is an absolute value<sup>58</sup>.

In order to minimize the influence of the spatial sensitivity distribution of the unfocused transducer, the PA signals of each vessel at the 578 nm and 588 nm optical illuminations were normalized by the PA amplitude of the same vessel acquired at the isosbestic wavelength of 570 nm.

**Vessel diameter and cross section area measurements.** We measured the vessel diameter axially in the OCT B-scan amplitude image, because of the high axial resolution of OCT. If we denote the vessel diameter in the B-scan as  $Dia$  [m], the actual vessel diameter  $Dia_r$  [m] is

$$Dia_r = Dia \times \sin(\theta) \quad (5)$$

where  $\theta$  [radians] is the Doppler angle. The vessel cross-sectional area  $A$  [m<sup>2</sup>] is calculated by

$$A = \pi \times \frac{Dia_r^2}{4}. \quad (6)$$

**Blood velocity and flow rate**

In Doppler OCT, the probing light passes through the pupil lens and is focused onto retinal vessels. The blood velocity  $v$  [m/s] can be calculated as

$$v = \frac{f_{\text{sample}} \cdot \lambda_0 \cdot \Delta\phi}{4 \cdot \pi \cdot n \cdot \cos(\theta)}, \quad (7)$$

where  $f_{\text{sample}}$  [kHz] is the SD-OCT A-line rate;  $\lambda_0$  [nm] is the center wavelength of the SD-OCT light source;  $\Delta\phi$  is the phase shift [degree] between adjacent OCT A-lines after bulk motion correction<sup>59</sup>;  $n$  [dimensionless] is the refractive index of the sample ( $n=1.4$ ); and  $\theta$  [radians] is the Doppler angle (estimation of the Doppler angle can be found in Supplementary Figure S4). To reduce the influence of eye motion on Doppler angle estimation, we averaged the estimated vessel depth across eight consecutive OCT B-scans. In our current work, the largest error in vessel depth is 2.9  $\mu\text{m}$  across eight B-scans. Considering the scanning radii difference between the outer- and inner-scanning rings is 110  $\mu\text{m}$ , the largest 2.9  $\mu\text{m}$  depth error results in an angle estimation error of 1.5 degrees. Since the mean value of the measured Doppler angle is around 82 degrees, the influence of the 1.5-degree angle error is small.

We observed the phase-wrap in retinal flow measurement. Phase-wrap can be corrected once we know the axial blood flow direction, which can be obtained from the phase value close to the vessel border since flow velocity near vessel wall is small enough to prevent phase-wrapping<sup>60</sup>. With the known blood flow direction and assuming the actual phase  $\Delta\phi < 0$ , we have

$$\Delta\phi = \begin{cases} \Delta\phi, & \Delta\phi < 0 \\ \Delta\phi - 2\pi, & \Delta\phi > 0 \end{cases} \quad (8)$$

after phase wrapping correction. If the actual phase is  $\Delta\phi > 0$ , we have

$$\Delta\phi = \begin{cases} \Delta\phi, & \Delta\phi > 0 \\ \Delta\phi + 2\pi, & \Delta\phi < 0 \end{cases} \quad (9)$$

after phase wrapping correction. After the blood velocity and vessel size are obtained, the blood flow in the  $i_{th}$  vessel is

$$F_i = v_i \times A_i, \quad (10)$$

where  $v_i$  is the average velocity and  $A_i$  is the vessel cross-sectional area.

**Retinal metabolic rate of oxygen (rMRO<sub>2</sub>).** The rMRO<sub>2</sub> [g/min] is quantified as

$$\begin{aligned} rMRO_2 &= \frac{60 \times 4 \times W_{O_2}}{W_{HbO_2}} \times [HbT] \times (sO_{2a} \times F_a - sO_{2v} \times F_v) \\ &= \frac{60 \times \pi \times W_{O_2}}{W_{HbO_2}} \times [HbT] \times \left( \sum_{i=1}^M sO_{2ai} \times d_{ai}^2 \times v_{ai} - \sum_{i=1}^N sO_{2vi} \times d_{vi}^2 \times v_{vi} \right), \end{aligned} \quad (11)$$

where  $W_{O_2}$  and  $W_{HbO_2}$  are the molecular weights of  $O_2$  and oxyhemoglobin, which are 32 and 68000 [g/mol], respectively;  $[HbT]$  is the total concentration of hemoglobin in the rat, which is 150 [g/L] in current studies;  $sO_{2ai}$  and  $sO_{2vi}$  are  $sO_2$  values in the  $i_{th}$  artery and vein, respectively;  $d_{ai}$  and  $d_{vi}$  are the vessel diameter of  $i_{th}$  artery and vein, respectively;  $v_{ai}$  and  $v_{vi}$  are the blood flow velocity within the  $i_{th}$  artery and vein, respectively;  $M$  and  $N$  are the number of arteries and veins, respectively. The standard deviation of rMRO<sub>2</sub> [g/min] ( $rMRO_{2\_std}$ ) is derived through the principle of error propagation as follows.

$$\begin{aligned} rMRO_{2\_std} &= \frac{60 \times \pi \times W_{O_2}}{W_{HbO_2}} \times [HbT] \times \text{sqr}t \left( \sum_{i=1}^N ((std(sO_{2ai}) \times d_{ai}^2 \times v_{ai})^2 \right. \\ &\quad \left. + (2 \times d_{ai} \times std(d_{ai}) \times sO_{2ai} \times v_{ai})^2 + (d_{ai}^2 \times sO_{2ai} \times std(v_{ai}))^2) \right) \\ &\quad + \sum_{i=1}^M ((std(sO_{2vi}) \times d_{vi}^2 \times v_{vi})^2 + (2 \times d_{vi} \times std(d_{vi}) \times sO_{2vi} \times v_{vi})^2 \\ &\quad \left. + (d_{vi}^2 \times sO_{2vi} \times std(v_{vi}))^2) \right), \end{aligned} \quad (12)$$

where  $std(\cdot)$  denotes the standard deviation operator and  $\text{sqr}t(\cdot)$  denotes the square root operator. The unit of rMRO<sub>2</sub> in Eq. 11 and Eq. 12 is ng/min, and we can convert ng/min to L/min by

$$V = n_g \times R \times T / P, \quad (13)$$

where  $V$  is the volume of gas;  $n_g$  is the number of moles of gas;  $R$  is 8.3145 [J·mole<sup>-1</sup>·K<sup>-1</sup>];  $T$  is the blood temperature (311.15 K); and  $P$  is the standard atmospheric pressure (101,325 Pa). All measured data, including vessel size,  $sO_2$ , and flow velocity, are given in Supplemental Table S2.

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## Author contributions

H.F.Z. and S.L.J. initiated the project. H.F.Z. supervised the project. W.S., Q.W., W.Z.L. and T.L. performed the experiments and analyzed the results. W.S., Q.W., W.Z.L., T.L., J.Y., N.S., A.A.F., R.A.L., S.L.J. and H.F.Z. discussed the results and contributed to the manuscript.

## Additional information

**Supplementary information** accompanies this paper at <http://www.nature.com/scientificreports>

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